

# Numerical Analysis of Propeller-induced Low-frequency **Modulations** in Underwater Electric Potential **Signatures** of Naval Vessels in the Context of **Corrosion Protection** Systems

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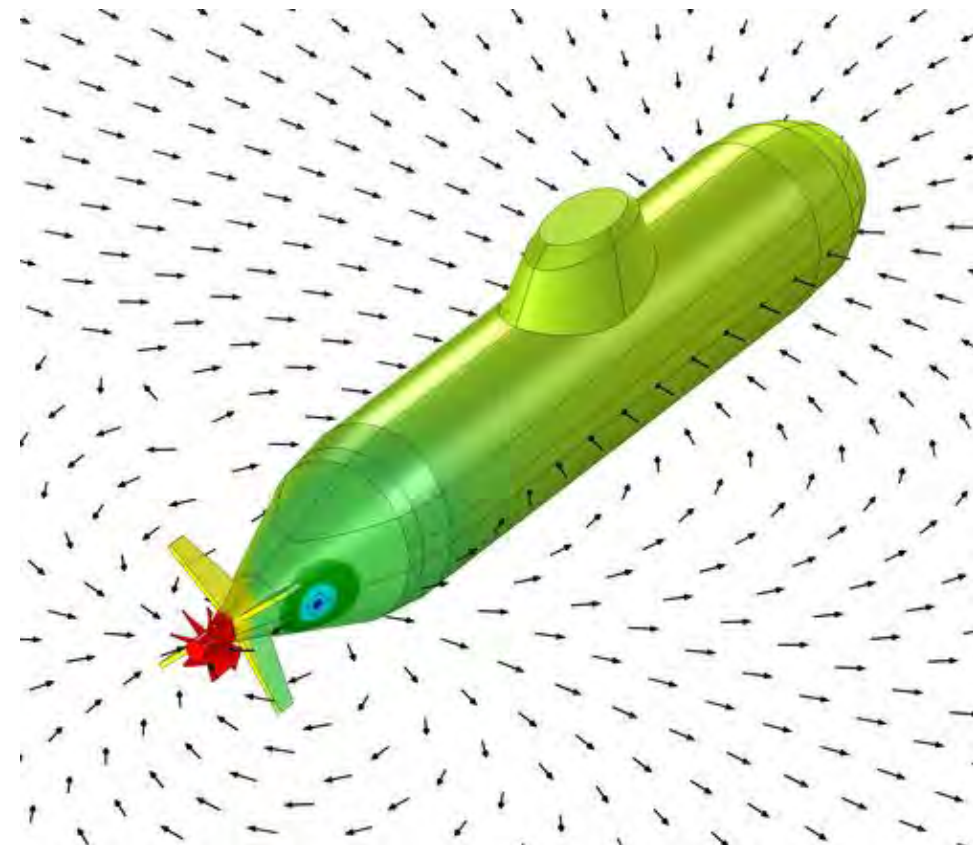
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# Outline

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  - Corrosion protection (CP) systems
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# Introduction (I)

## Underwater signatures and “Mine warfare” (MIW)

- The term “signature” originally referred to acoustic measurements of a vessel's underwater sound pressure field [1, p.1ff].
- Different types of signatures:
  - Acoustic signature
  - Magnetic signature
  - Electric signature (UEP signature)
  - ...
- Vessels (unintentionally) reveal their presence to their environment.
- Signatures exploited in “Mine warfare” (MIW) and “Anti-submarine warfare” (ASW).
- Naval influence mines buried in seabed can monitor signatures and actuate without direct contact.
- Acoustic and magnetic signatures well under control.
- Electric (UEP) signatures not so important until now, but probably in the future → **Focus of our research**



Diverse influence mines (*under CC-license; Author: Darkone@Wikipedia*)



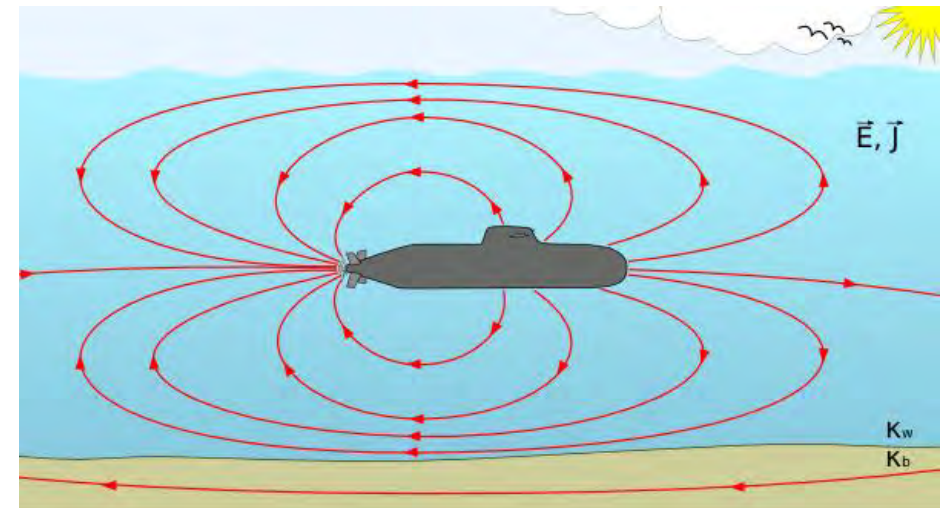
Acoustic influence mine found in the Arabian Gulf



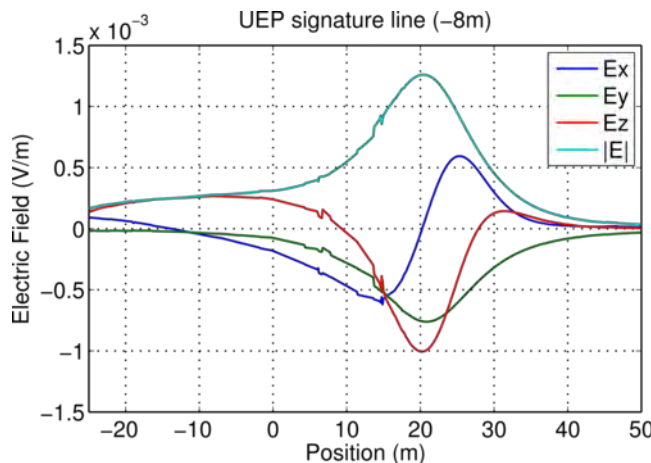
# Introduction (II)

## Underwater electric potential (UEP) signature

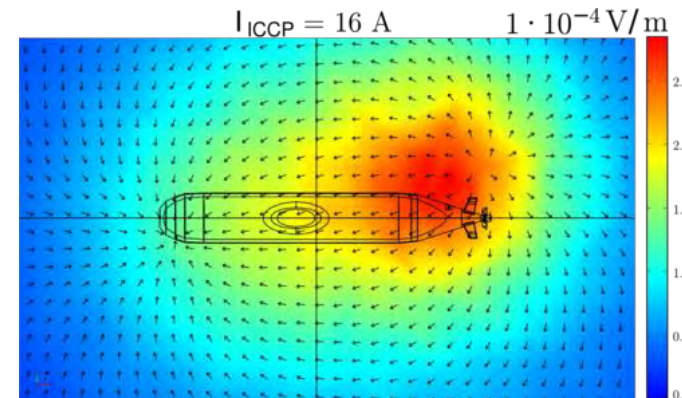
- Reasons for the electric currents in water:
  - Electrochemical reactions (Corrosion)
  - Corrosion protection systems
- Common representation for UEP signature:
  - “Signature line” (Axial trace)
  - “Signature plane” (Slice plot)



Sketch of typically electric current paths around a submarine.



Axial trace of the near-field (8m below the keel) UEP signature of a simplified submarine model, simulated with COMSOL.

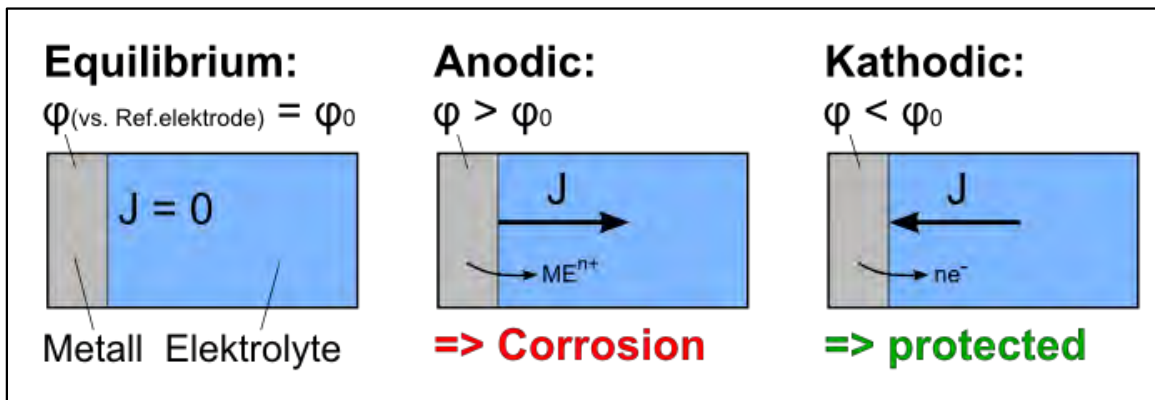


Signature plane of the electric field in a depth of 20m (66ft) below the keel, simulated with COMSOL.

# Introduction (III)

## Corrosion protection (CP) for naval vessels

- Active corrosion protection systems:
  - Galvanic/sacrificial anodes
  - Impressed current cathodic protection (ICCP) systems
- Active CP often based on cathodic currents:



- Passive corrosion protection:
  - Isolating coatings
  - Protective paintings
  - Proper material combination
- **Question:** What is the ideal corrosion protection setup to minimize the UEP signature?



Galvanic zinc anodes (under CC-license; Author: Hgrobe@Wikipedia)



Galvanic anodes placed on a ships hull

# COMSOL Multiphysics simulations

## Governing equations

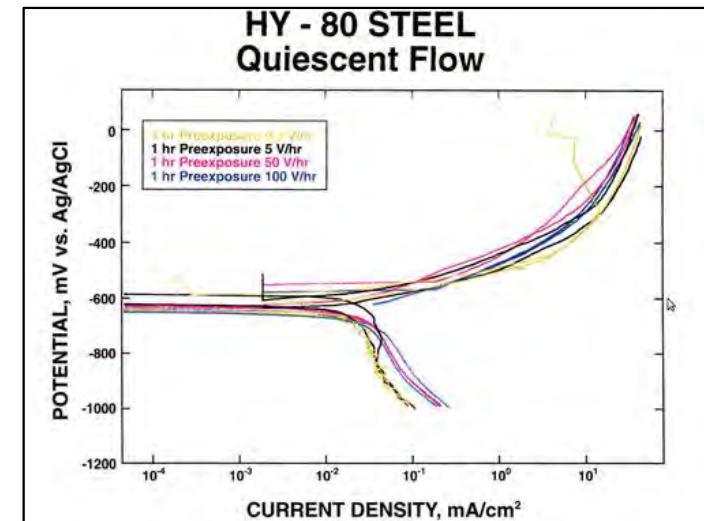
- Poisson equation (AC/DC Module – Electric Currents):  $\Delta(\sigma \cdot V) = 0$
- Electric field and current density:  $\vec{E} = -\nabla V$        $\vec{J} = \sigma \cdot \vec{E}$

## Electrode kinetics considering measured polarization curves

- Neumann boundary condition (“Inward current density”):  
 $\vec{n} \cdot \vec{J} = J_i(V)$
- $J_i(V)$  represents a nonlinear polarization curve.
- Simulated in COMSOL by using a piecewise interpolated function.

## Simulating via “LiveLink for Matlab”

- Capability to...
  - ...perform complex parameter sweeps.
  - ...implement customized optimization procedures.
- In-house developed toolbox to receive entity-ids by referring to the name-tag.

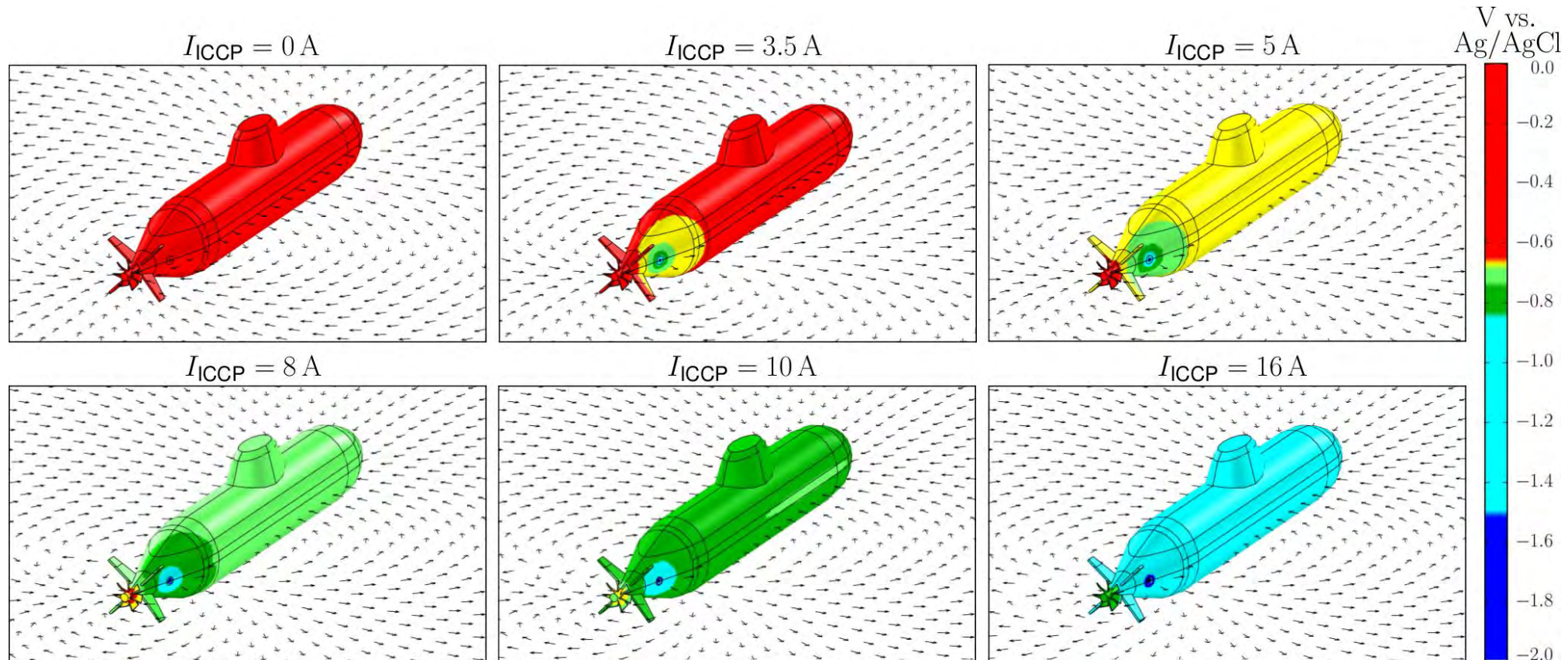


Polarization diagram measured by Hack [3].



# Research results (I)

## Potential distributions on the vessel's hull

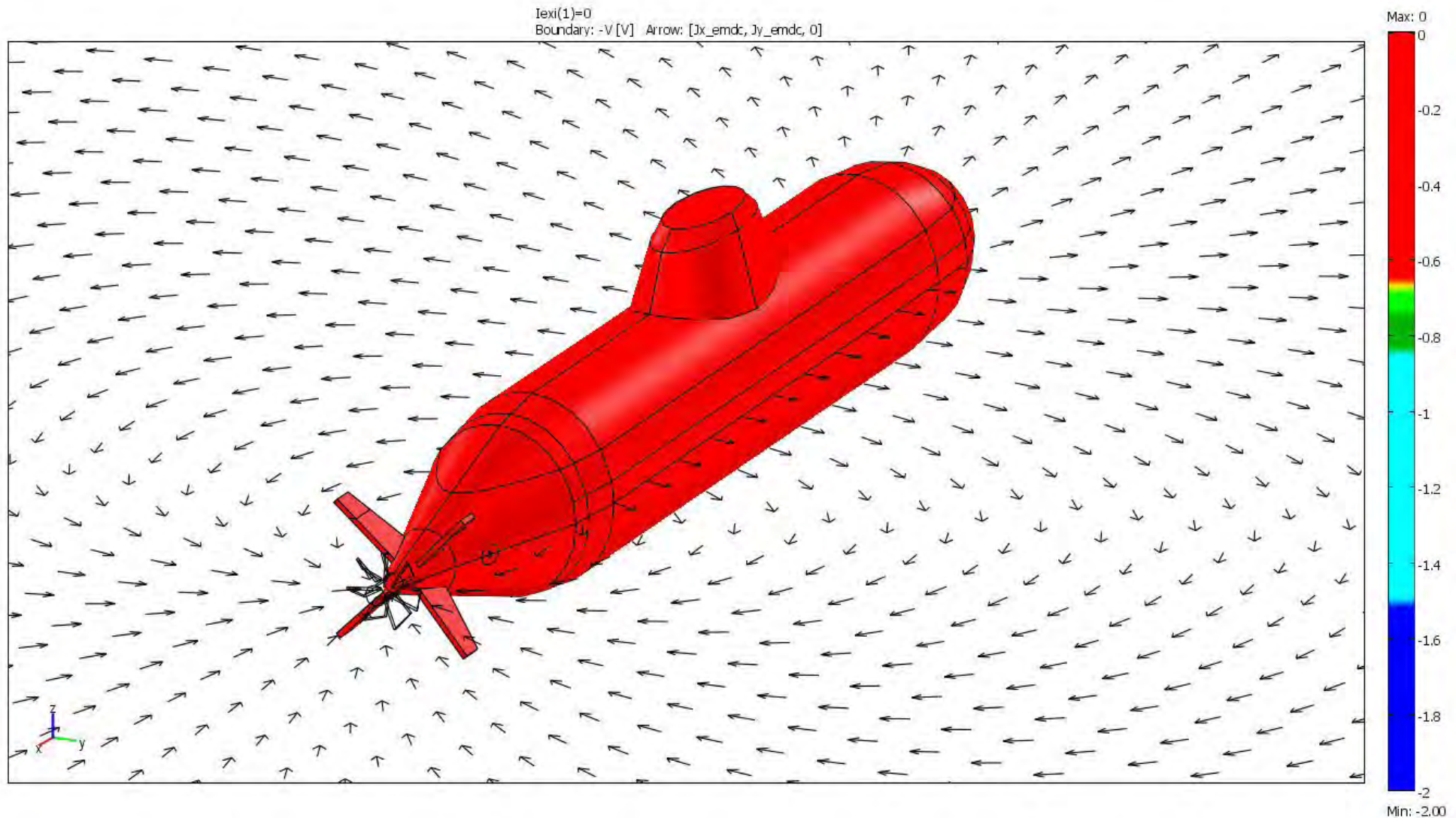


Potential distribution on the hull of a simplified submarine model, for different currents impressed by the ICCP system. The colorbar is based on the German naval directive "VG 81259" [2].

- Good protection at  $I_{ICCP} \approx 8\text{-}10\text{ A}$  for this submarine model.

# Research results (II)

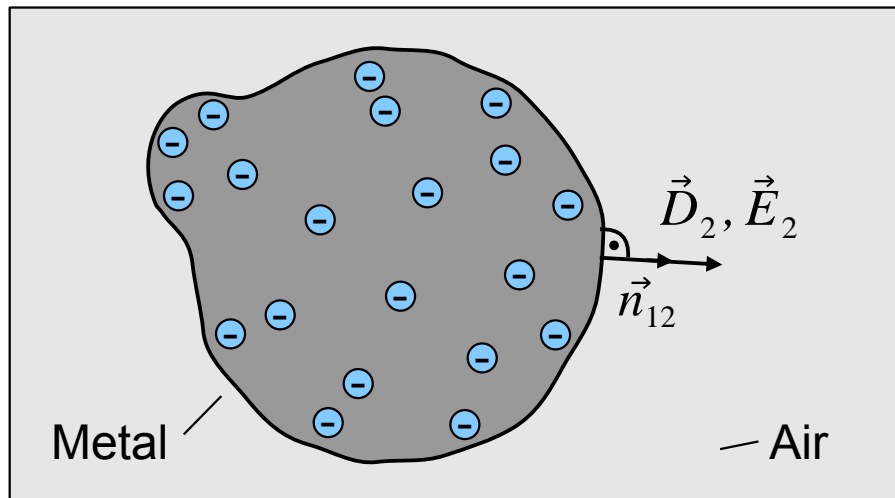
## Potential distributions on the vessel's hull





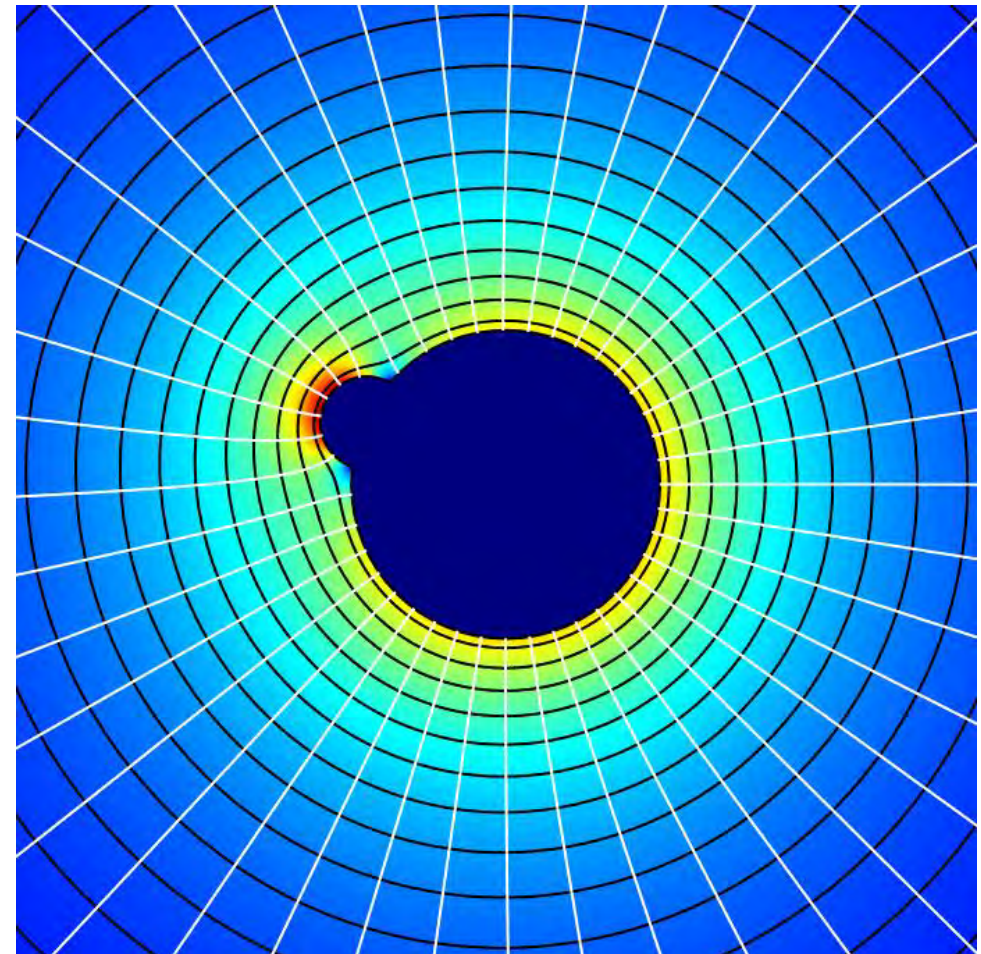
# Research results (III)

## Singular field peaks at sharp angles and edges



- Charges repel each other and move to the surface of the conductor.
- More charge on surface areas with small curvature (e.g. on buckles/angles/edges).
- Relation between  $\vec{D}$  and  $\sigma$  [4, S.102]:

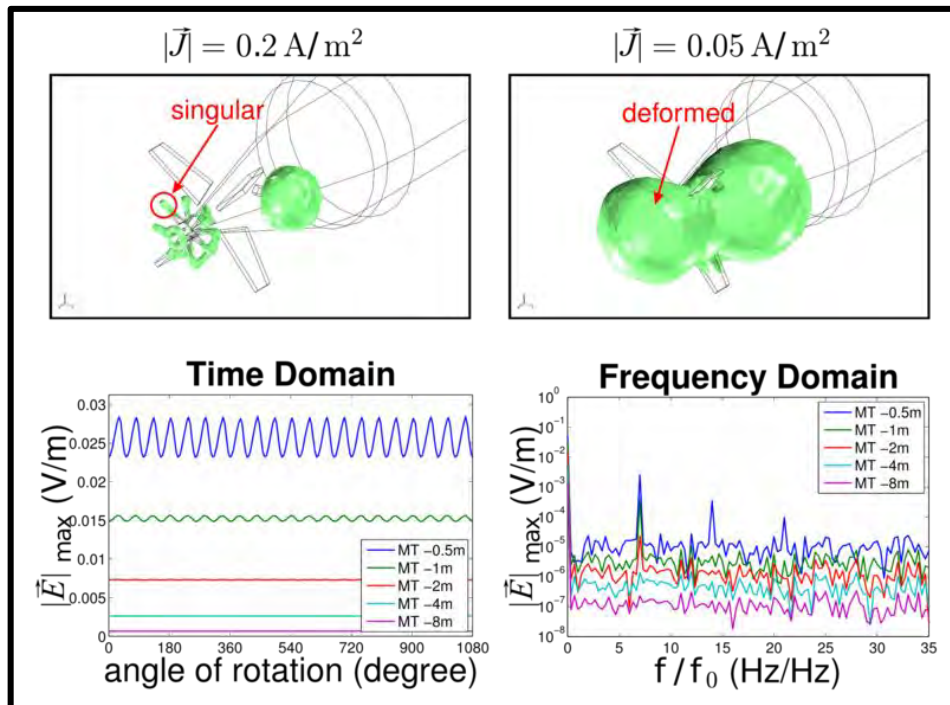
$$\vec{n}_{12} \cdot (\vec{D}_2 - \vec{D}_1) = \sigma \Rightarrow |\vec{D}_2| = \sigma$$



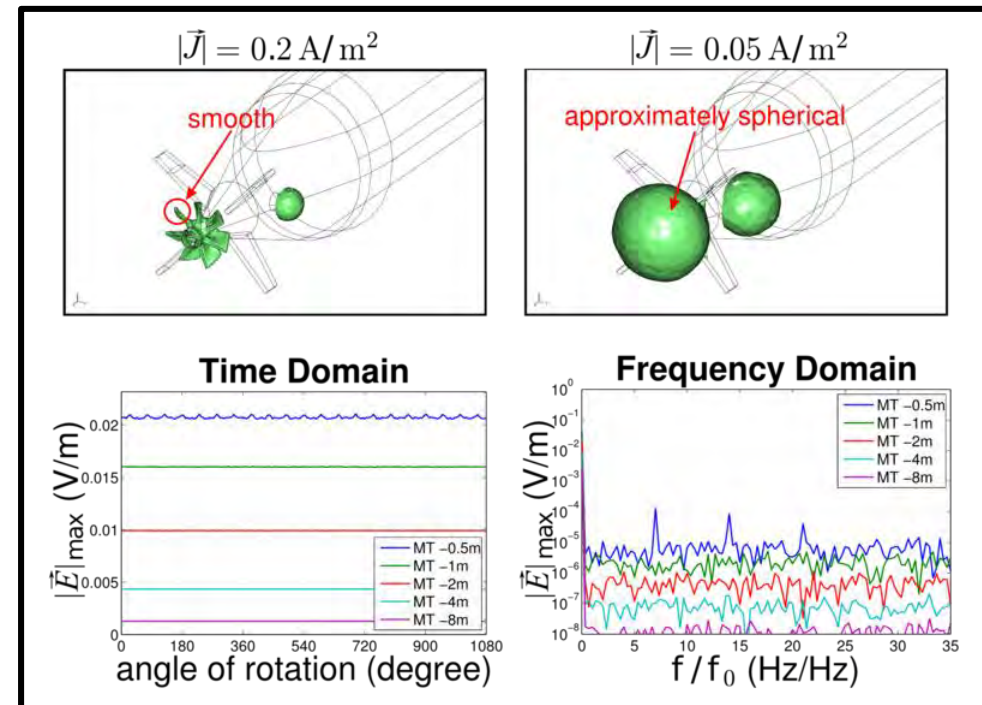
Field- and equipotential lines for an electrically charged "potato" simulated with COMSOL.

# Research results (IV)

## “Smoothing effect” of the polarization resistance



Simulated near-field modulation with **Dirichlet** boundary conditions.

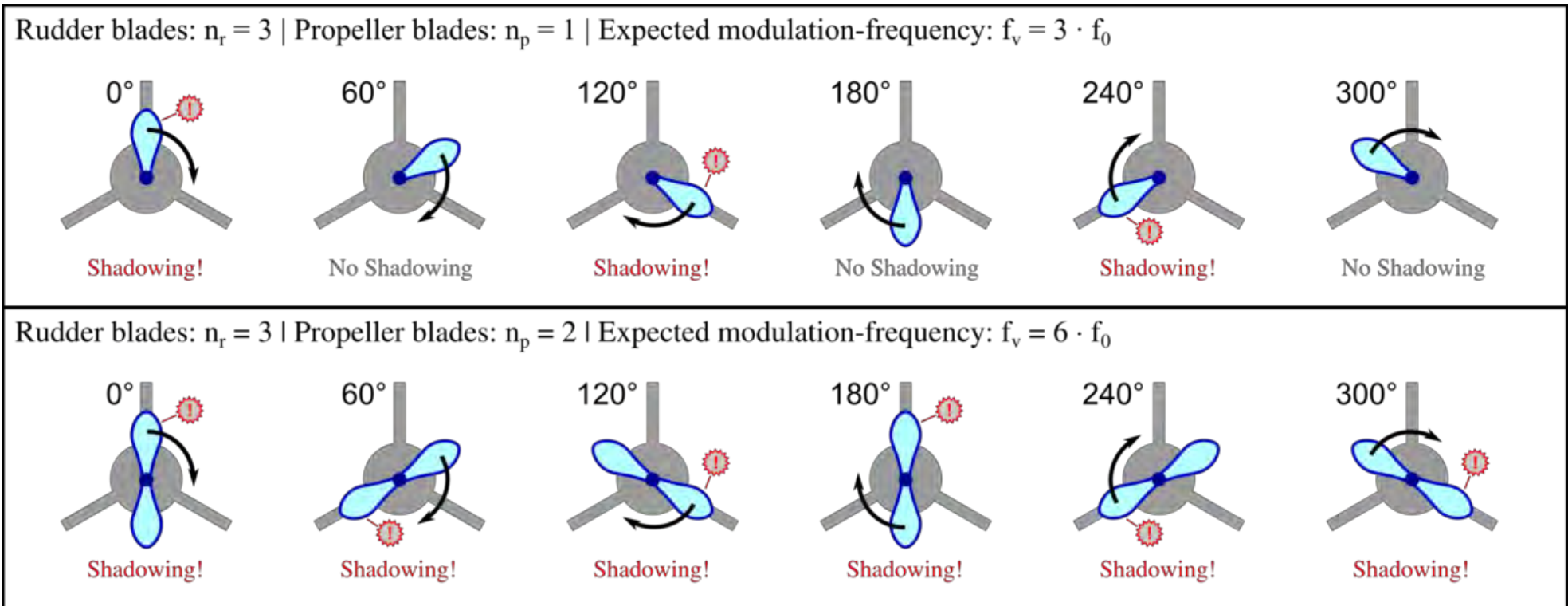


Boundary conditions based on **non-linear polarization curves**.

- Dirichlet: Singular field-peaks occur on sharp edges like the tips of the propeller blades.
- Rotating propeller modulates the electric near-field (rotating deformed equi-surfaces).
- Polarization resistance reduces the modulation (spherical equi-surfaces)

# Research results (V)

## Vernier-/Nonius effect



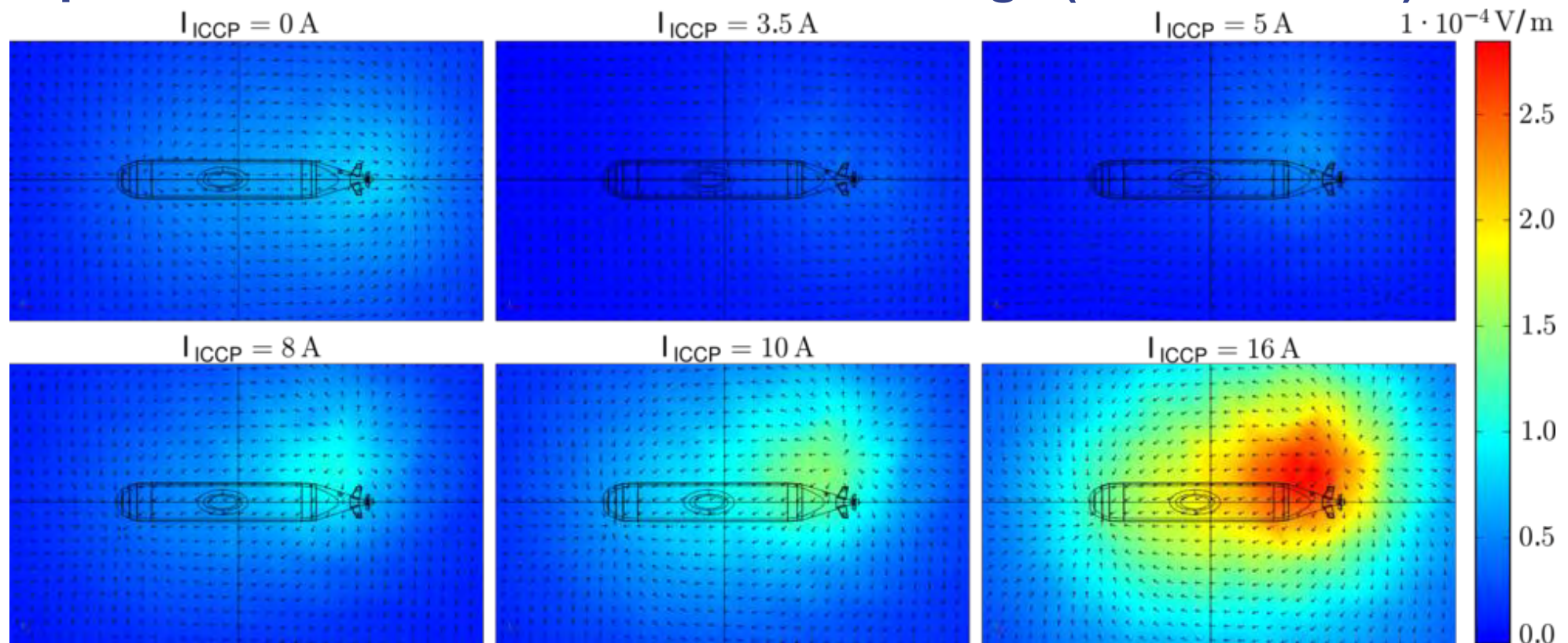
Theoretically example to illustrate the Vernier-/Nonius effect. The figure shows an astern view on a simplified submarine model.

- Propeller blades get covered behind rudder blades during the rotation of the propeller.
- **Question:** Does the total ICCP current become modulated?
- Frequencies corresponding to Vernier-/Nonius **not observable** in simulation.



# Research results (VI)

## Optimal ICCP current for “silent running” (stealth mode)



Signature planes of the electric field in a depth of 20m (66ft) below the keel, for different currents impressed by the ICCP system.

- Optimized ICCP currents can in fact reduce the UEP signature (**3.5A**).
- Switched off ICCP system does not necessarily produce the smallest UEP signature (**0A**).
- Overprotection can increase the UEP signature critically (**16A**).



# Conclusions and Outlook

## Conclusions

- COMSOL simulations provide us with a reliable basis for understanding the principally coherences in the application of UEP signatures.
- Polarization resistance “smoothens” singular field-peaks.
- Frequencies corresponding to Vernier-/Nonius effect not observable.
- Optimized ICCP currents can reduce UEP signature, but overprotection can increase the UEP signature critically.

## Outlook

- Simulations of the electric currents flowing back through the electron conductor (Using the COMSOL “Batteries & Fuel Cells Module”).
- Simulations of the corrosion related magnetic field.
- Qualitative changes in the UEP signature of scaled models.



# Literature

- [1] J. J. Holmes, "Exploitation of a Ship's Magnetic Field Signature", Morgan & Claypool Publishers, (2006).
- [2] BWB, VG 81259 Teil 1-3, "Kathodischer Korrosionsschutz von Schiffen – Außenschutz durch Fremdstrom", Beuth, (1994).
- [3] H. P. Hack, "Atlas of Polarization Diagrams for Naval Materials in Seawater", Carderock Division Naval Surface Warfare Center (1995).
- [4] Erni, D. : *Theoretische Elektrotechnik 1+2* (2010).
- [5] <http://wikipedia.org/>



Thank you for  
your attention!

Questions?

Meet me at my poster →

When? 17:30 – 19:30

Where? Bürgersaal-Foyer

(also you can find my paper in  
the conference proceedings)

**Numerical Analysis of Propeller-induced Low-frequency Modulations in Underwater Electric Potential Signatures of Naval Vessels in the Context of Corrosion Protection Systems**

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**1. Abstract**

Since October 2009 the laboratory of ATE has carried out collaborative research with the WTD 71, that aims for prediction, reduction and optimization of so-called underwater electric potential (UEP) signatures. For submarines and other naval vessels (e.g. minesweepers) a minimal UEP signature is vital to prevent the detection by underwater barriers. In the context of impressed current cathodic protection (ICCP) systems we numerically simulate potential distributions on the vessels hulls, in order to obtain the corresponding UEP signatures. For this purpose we use COMSOL Multiphysics with 'LiveLink for Matlab' and 'AC/DC Module' (laterly also 'Batteries & Fuel Cells Module'). The electrochemical behavior of the coated hull in seawater is considered by using boundary conditions based on non-linear polarization curves.

**2. Potential distribution on a submarine hull**

**3. Propeller-induced modulation by means of shadowing effects**

**4. Vernier-Nonius Effect**

**5. Electric field below the keel**

**6. Conclusions**

- Polarization resistance at interface between electronic conductors flattens singular field-peaks at sharp edges → reduction of the propeller-induced low-frequency modulations of UEP signatures.
- Propeller-induced modulation of the total ICCP current by means of shadowing effects is negligible. Frequencies corresponding to Vernier-Nonius effect are not observable ( $f = \text{form}(\omega) \cdot \omega = \text{form}(\omega) \cdot \omega$ ).
- Wave-correlation related UEP signature (switched-off ICCP) can be less-, but in some cases even more intense than UEP signature including ICCP system.

**7. Literature**

[1] NAGA, H. P.: Atlas of Polarization Diagrams for Naval Materials in Seawater / Castorack Division Naval Surface Warfare Center, 1995. – Forschungsbericht  
[2] GRW: VG 81 259 Teil 1-3. Kathodischer Korrosionsschutz von Schiffen. Ausschusschutz durch Fremdbatterien. (Norn), 2004.

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