



Dynamic Simulation of Electromagnets

European COMSOL Conference

5 November 2008

Contents

1. Electronic brake systems by Continental Automotive Systems
 - ▶ ABS
 - ▶ ESC
2. COMSOL for electromagnetic actuators
 - ▶ Magnetic force
 - ▶ Armature movement by mesh deformation
 - ▶ Fast calculation of system dynamics
3. Conclusion

Contents

1. Electronic brake systems by Continental Automotive Systems
 - ▶ ABS
 - ▶ ESC
2. COMSOL for electromagnetic actuators
 - ▶ Magnetic force
 - ▶ Armature movement by mesh deformation
 - ▶ Fast calculation of system dynamics
3. Conclusion

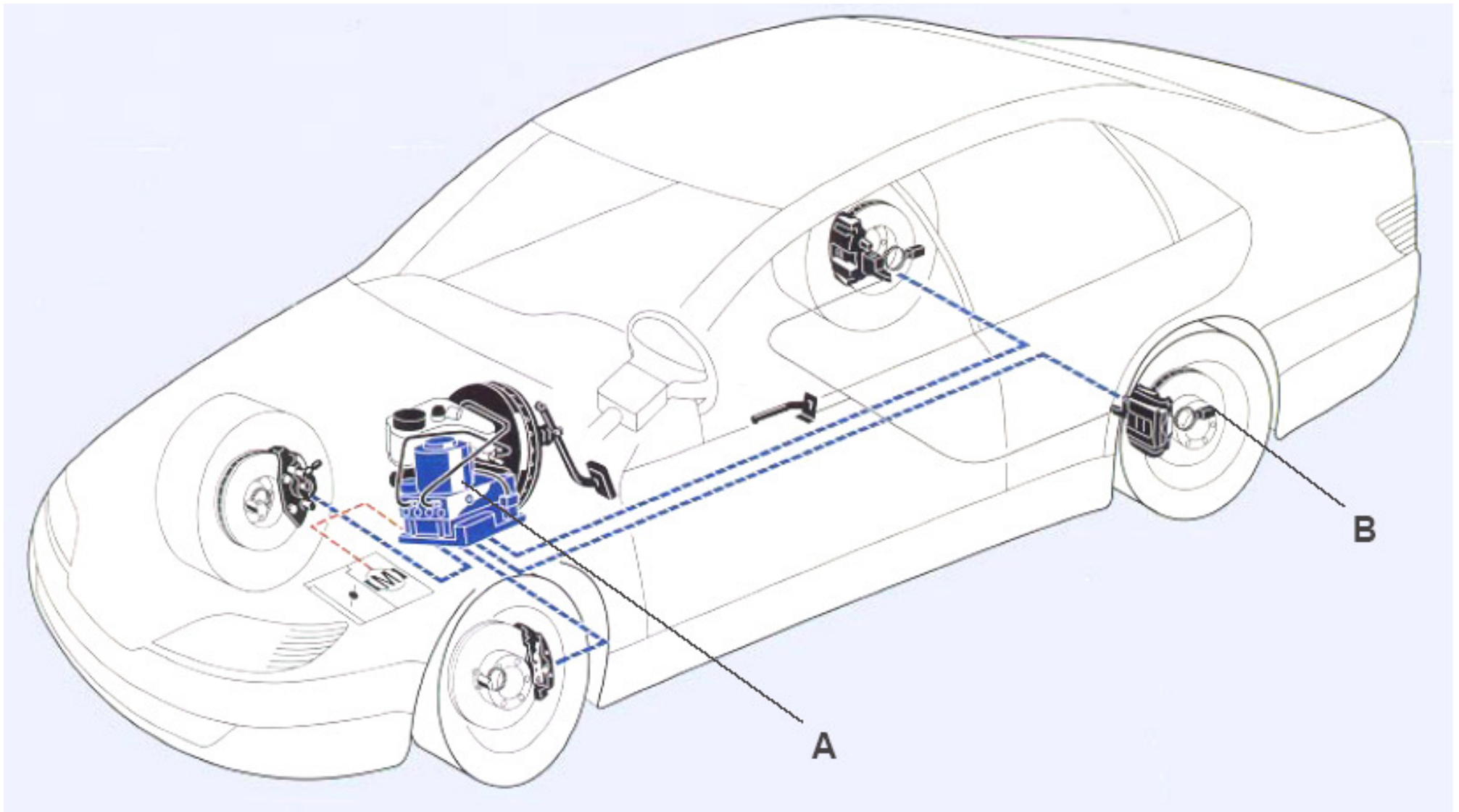
Anti-lock brake system (ABS)

- ▶ control slip between wheel and road
- ▶ “stick friction > slip friction”
- ▶ maximize force between wheel and road
- ▶ maintain lateral guiding force

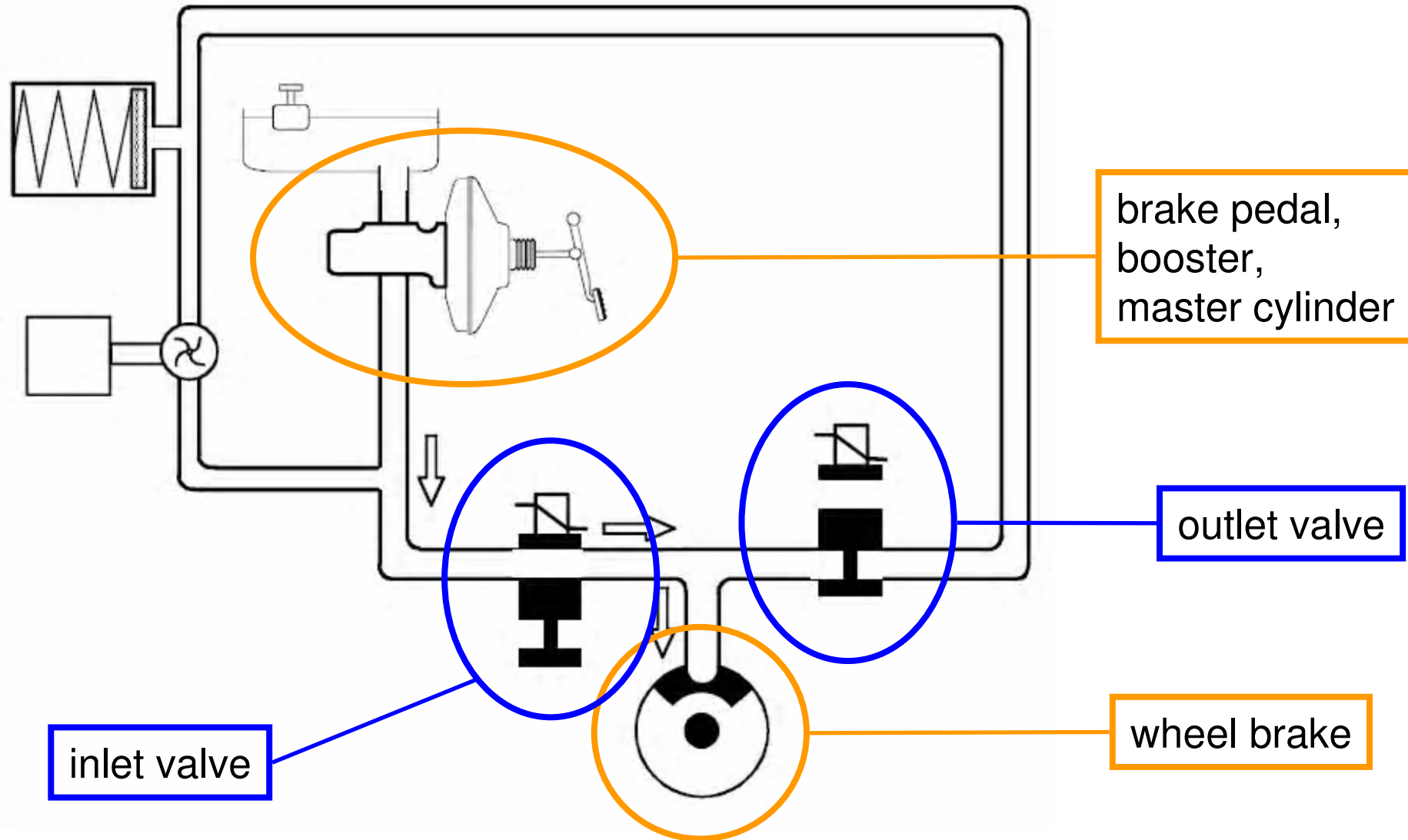
targets:

- ▶ vehicle remains stable
- ▶ vehicle can be steered
- ▶ shorter stopping distance in most situations

ABS components

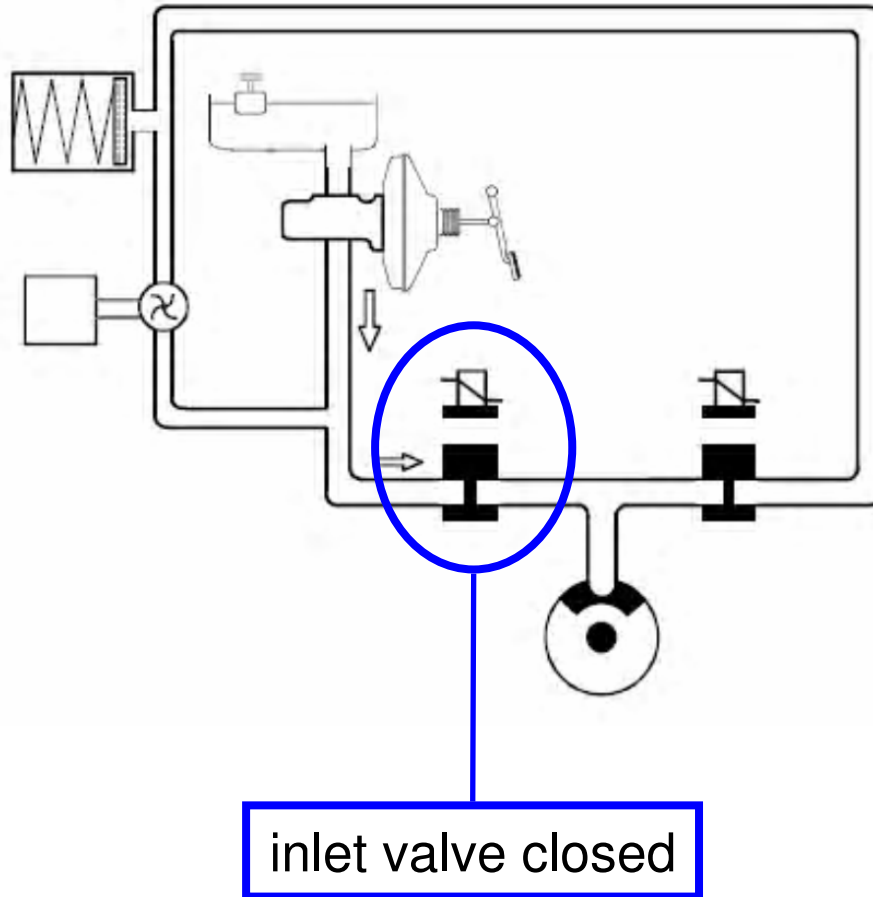


ABS hydraulic layout

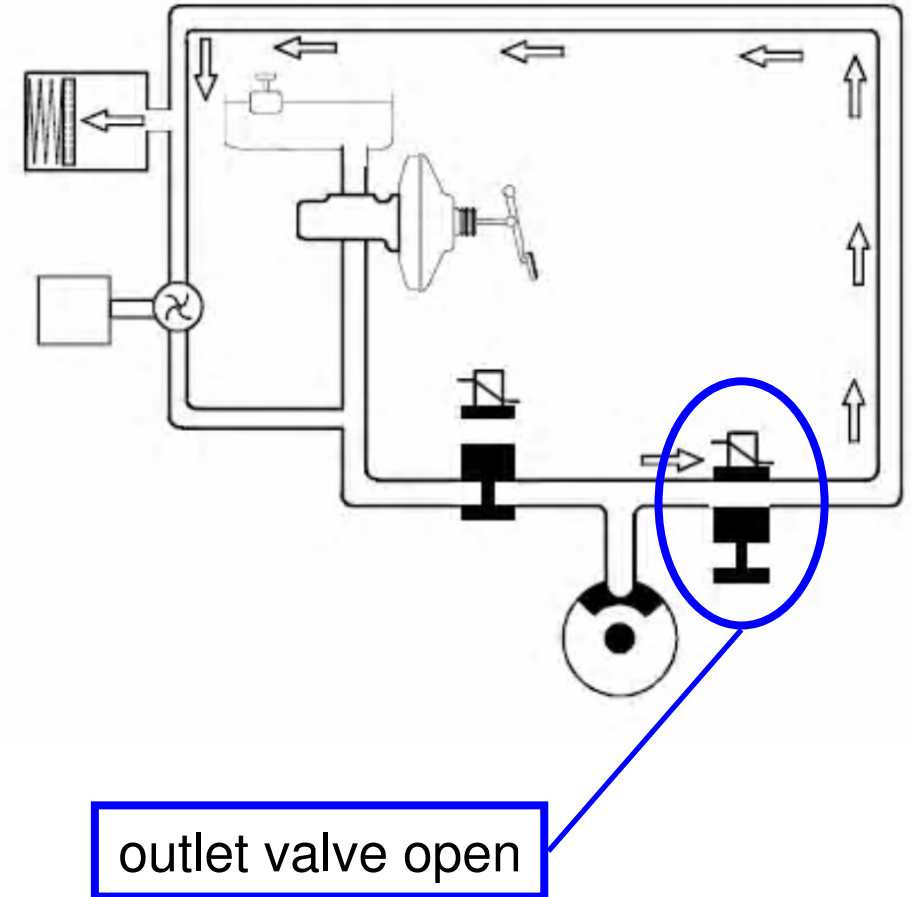


ABS active control

constant pressure phase



pressure decrease phase



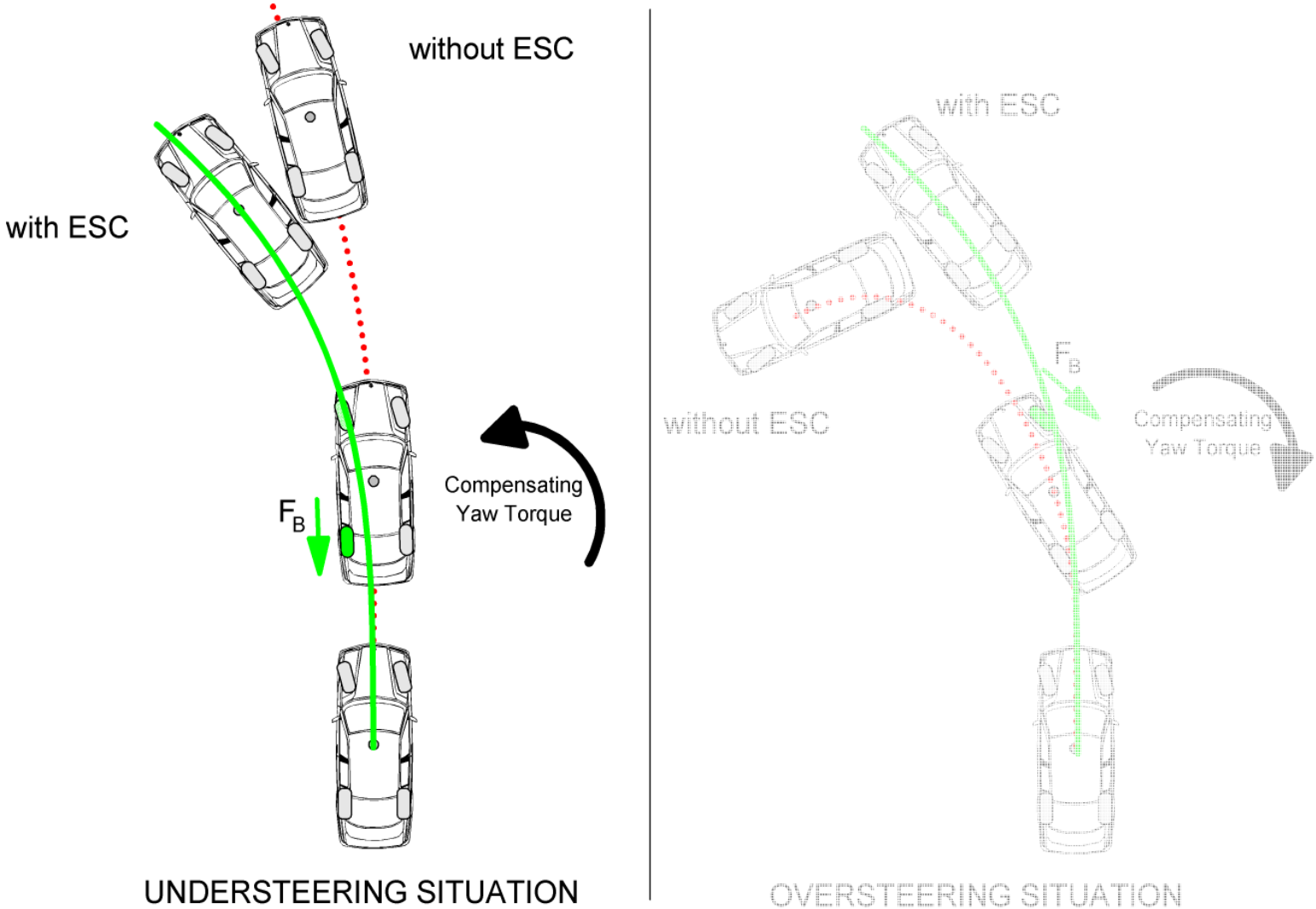
Antilock Brake System ABS – μ -Split Braking



Antilock Brake System ABS – μ -Split Braking

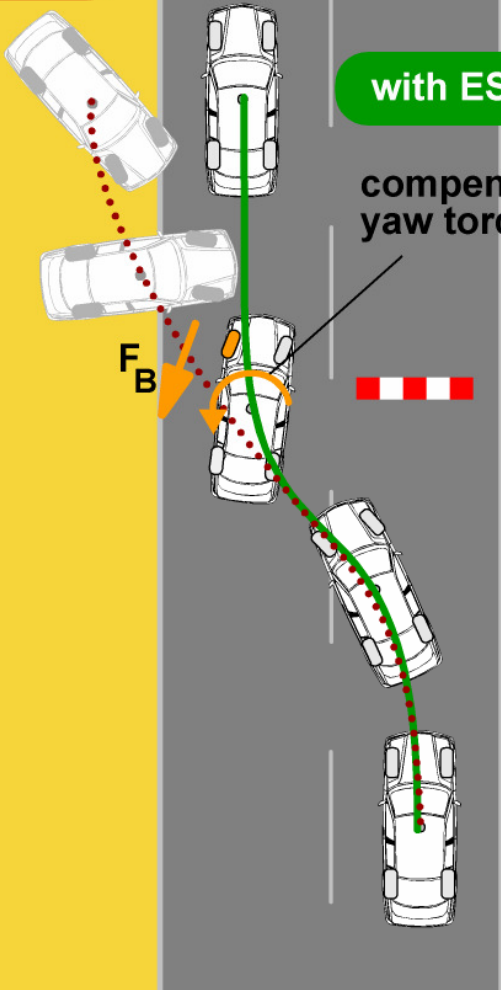


Electronic Stability Control ESC – Active Yaw Control



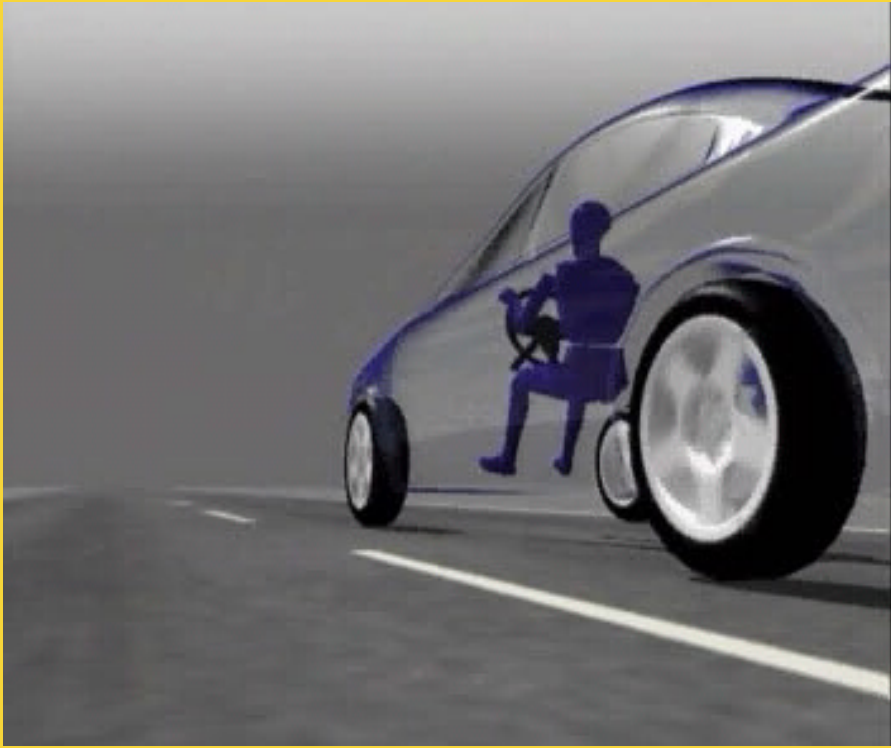
Electronic Stability Control ESC

without ESC



with ESC

compensating yaw torque



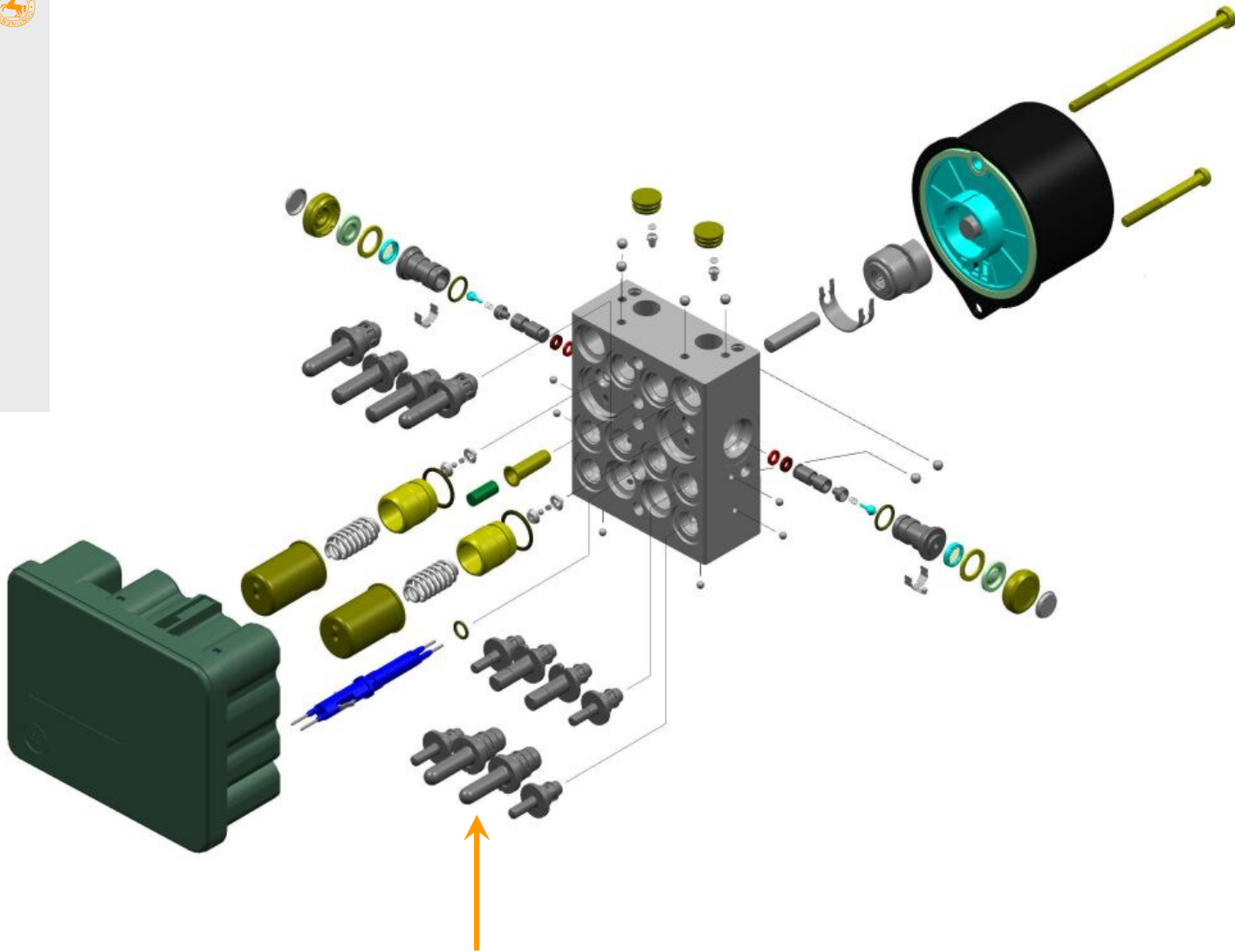
- + ABS: Anti-lock Brake System
- + EBD: Electronic Brake force Distribution
- + TCS: Traction Control System
- + AYC: Active Yaw Control

- = ESC: Electronic Stability Control

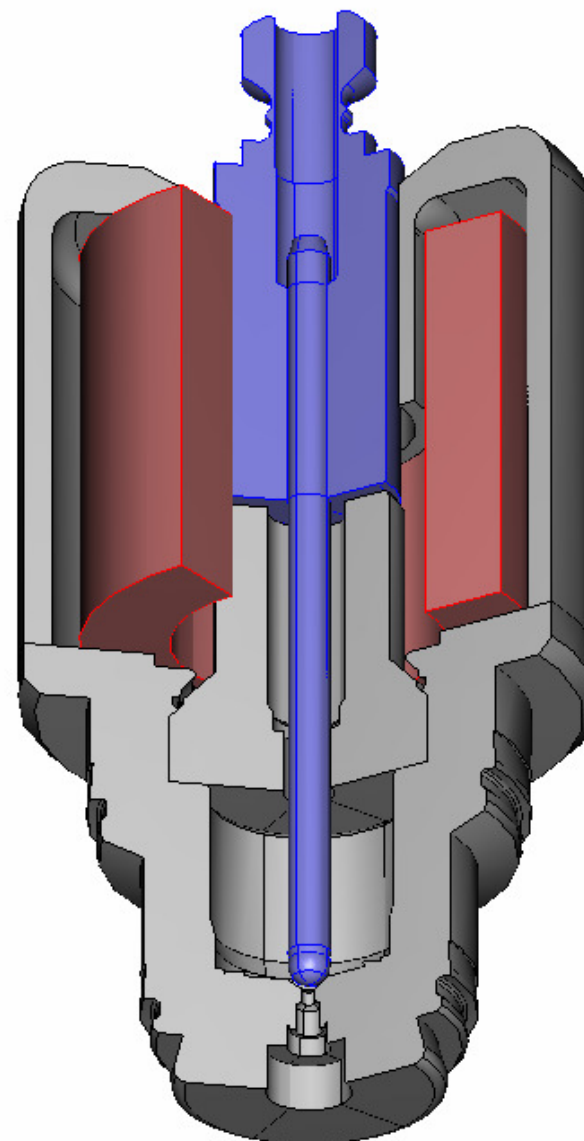
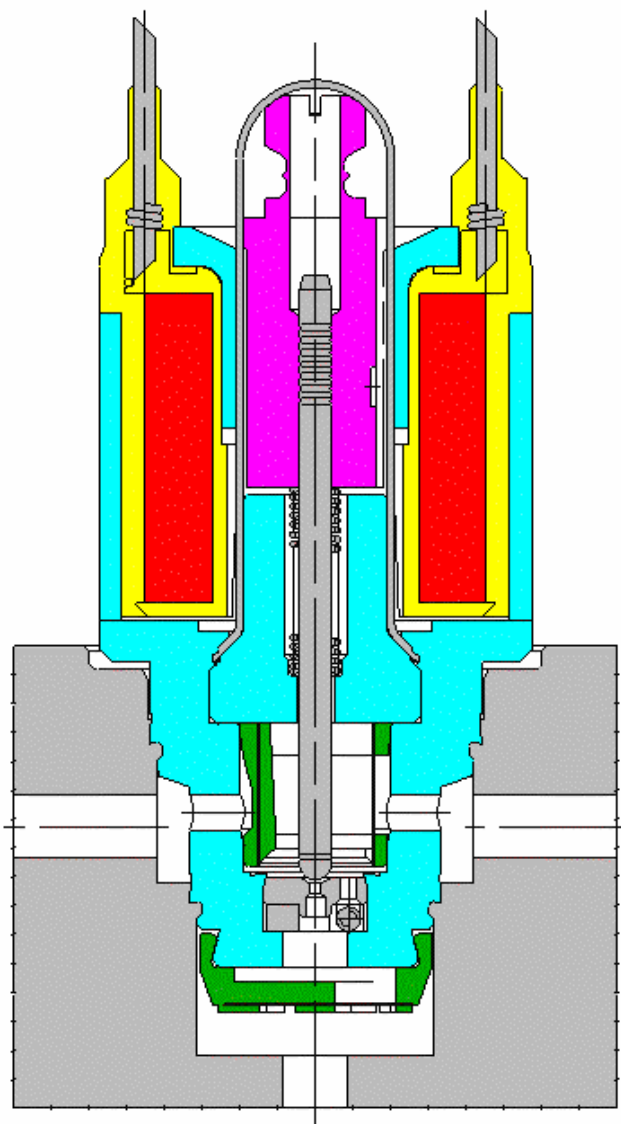
Contents

1. Electronic brake systems by Continental Automotive Systems
 - ▶ ABS
 - ▶ ESC
2. COMSOL for electromagnetic actuators
 - ▶ Magnetic force
 - ▶ Armature movement by mesh deformation
 - ▶ Fast calculation of system dynamics
3. Conclusion

Electronic Stability Control ESC – Exploded View

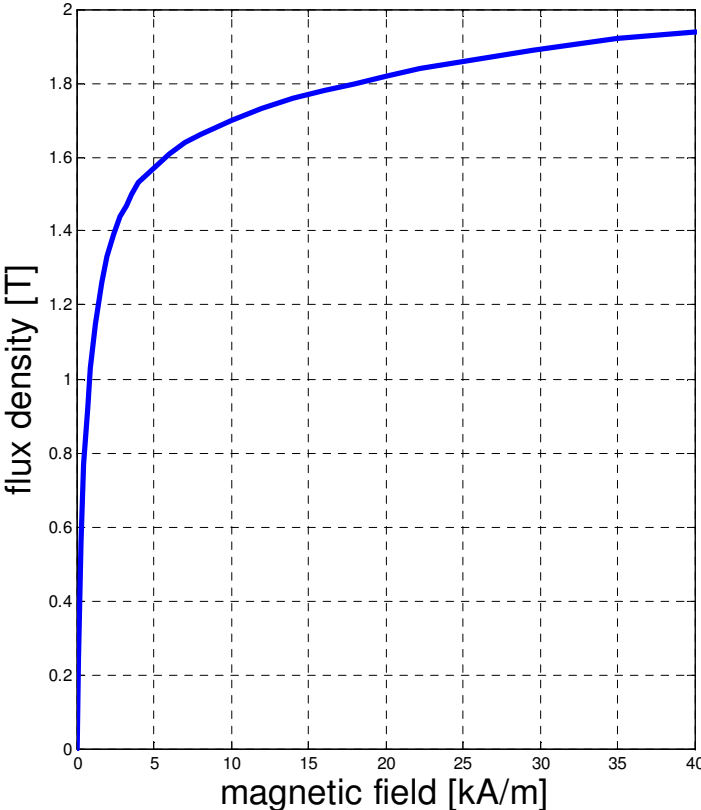


Electromagnetic inlet valve



Magnetization of steel

magnetic field $\vec{H} = \frac{1}{\mu_0 \mu_r} \vec{B}$ magnetic flux density



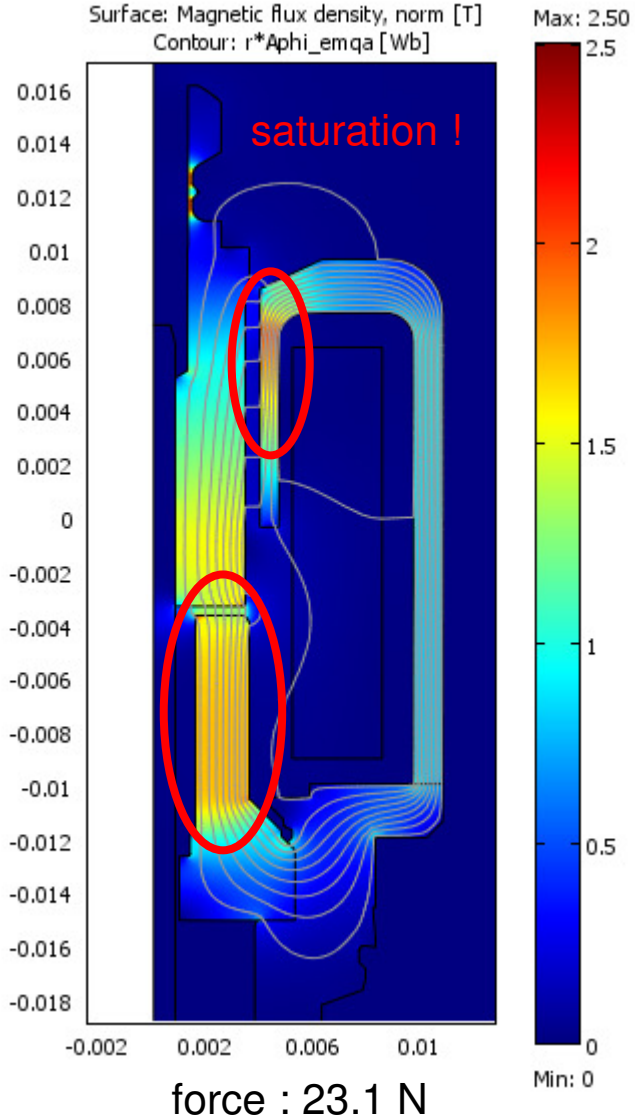
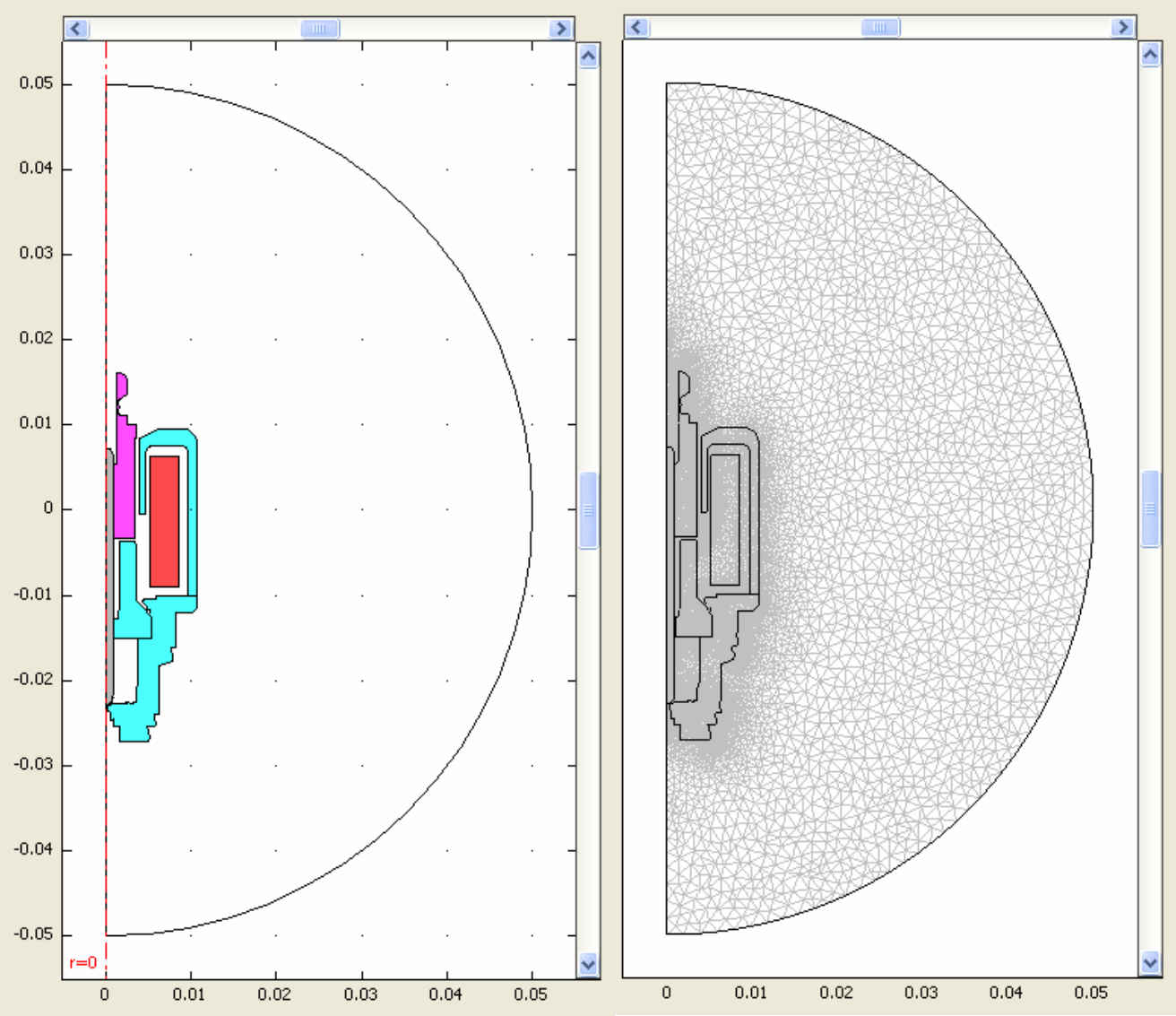
COMSOL > Physics > Subdomain Settings

Quantity	Value/Expression	Unit	Description
\mathbf{v}	0	m/s	Velocity
V_{loop}	0	V	Loop potential
\mathbf{j}^e_ϕ	0	A/m ²	External current density
σ	0	S/m	Electric conductivity
$\mathbf{H} \leftrightarrow \mathbf{B}$	$\mathbf{B} = \mu_0 \mu_r \mathbf{H}$		Constitutive relation
μ_r	<code>mu_r(normB_qa)</code>	1	Relative permeability

COMSOL > Physics > Equation System > Subdomain Settings

`normB_qa = sqrt(eps + abs(Br_qa)^2 + abs(Bz_qa)^2)`

Materials, mesh, solution

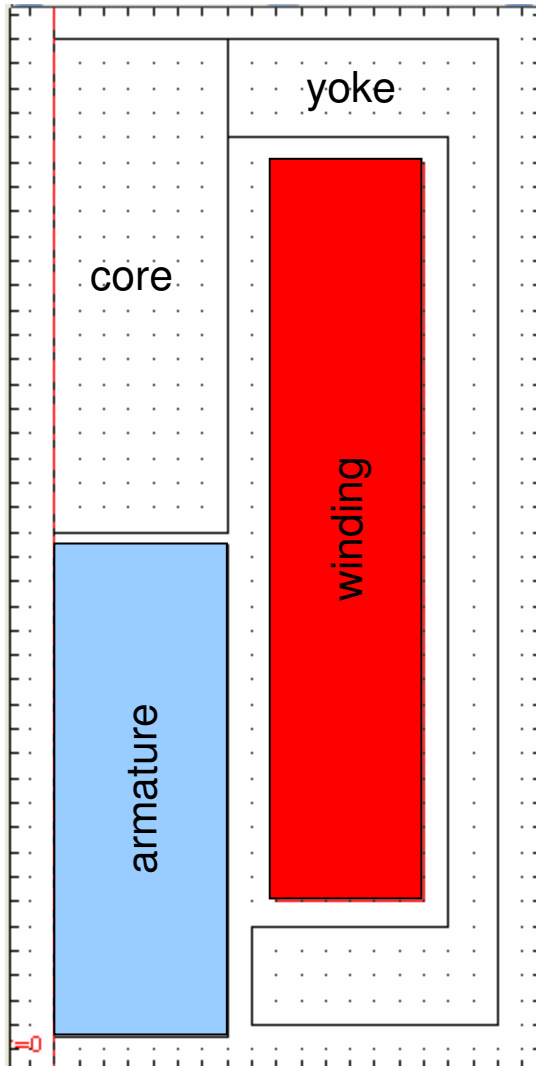


Contents

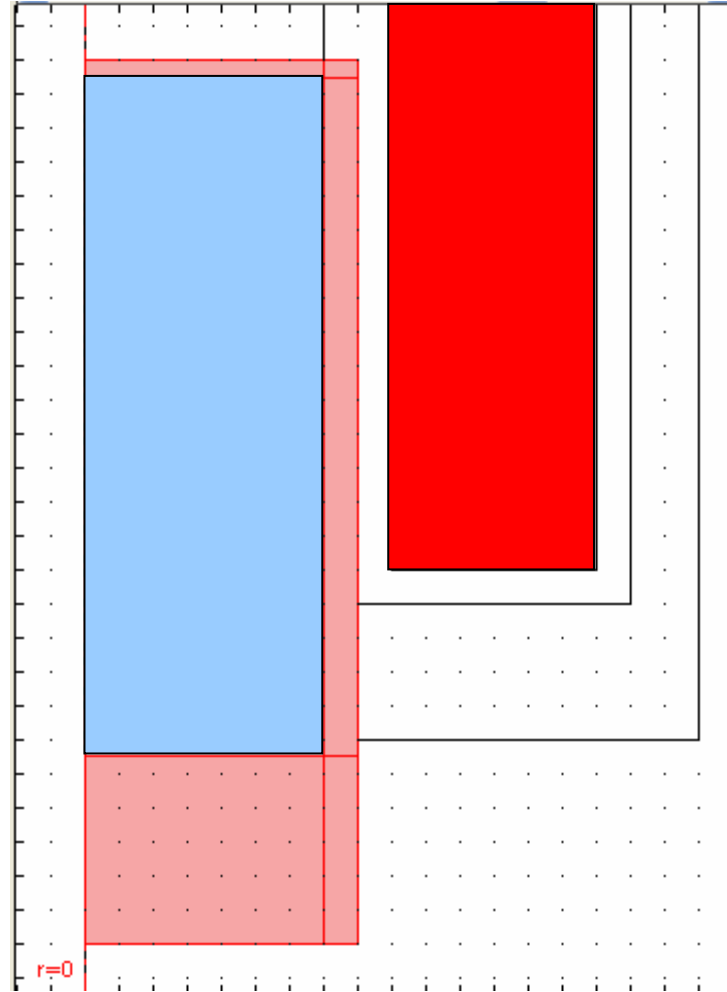
1. Electronic brake systems by Continental Automotive Systems
 - ▶ ABS
 - ▶ ESC
2. COMSOL for electromagnetic actuators
 - ▶ Magnetic force
 - ▶ Armature movement by mesh deformation
 - ▶ Fast calculation of system dynamics
3. Conclusion

Geometry and deformation domain

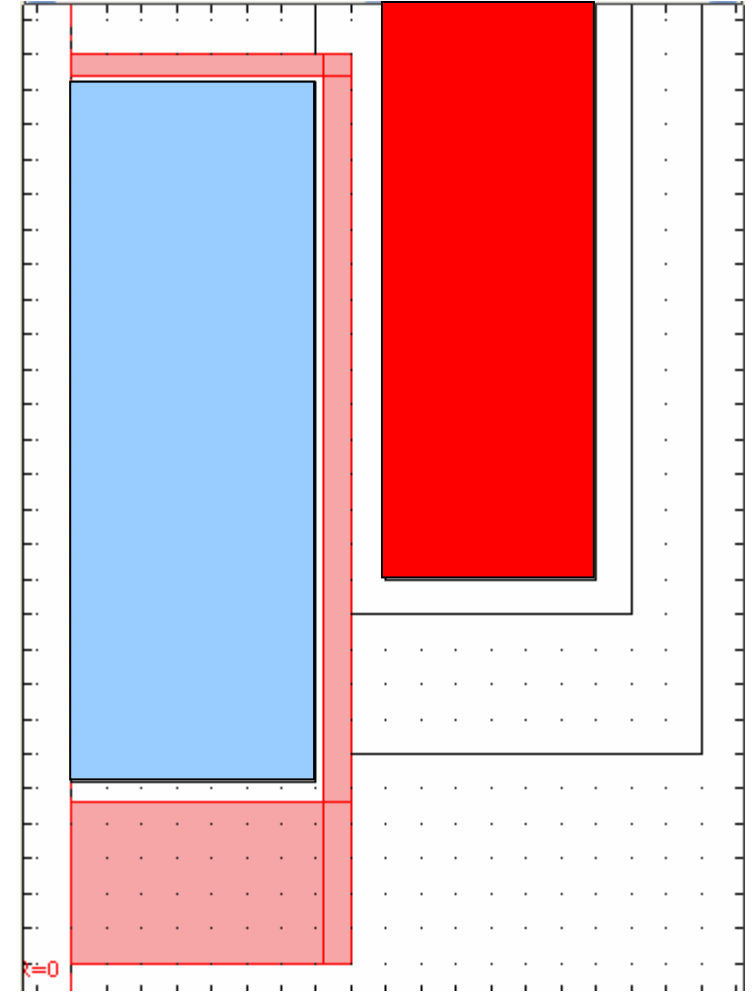
simplified geometry



armature with deformation domain

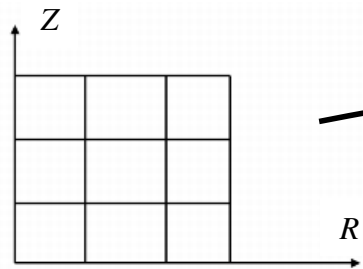


armature with rigid hull

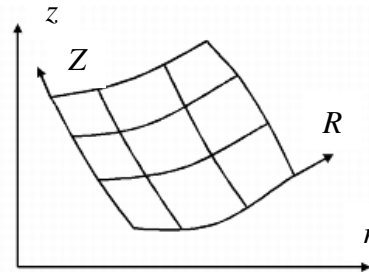


Idea of ALE (“arbitrary Lagrangian-Eulerian”) mesh deformation

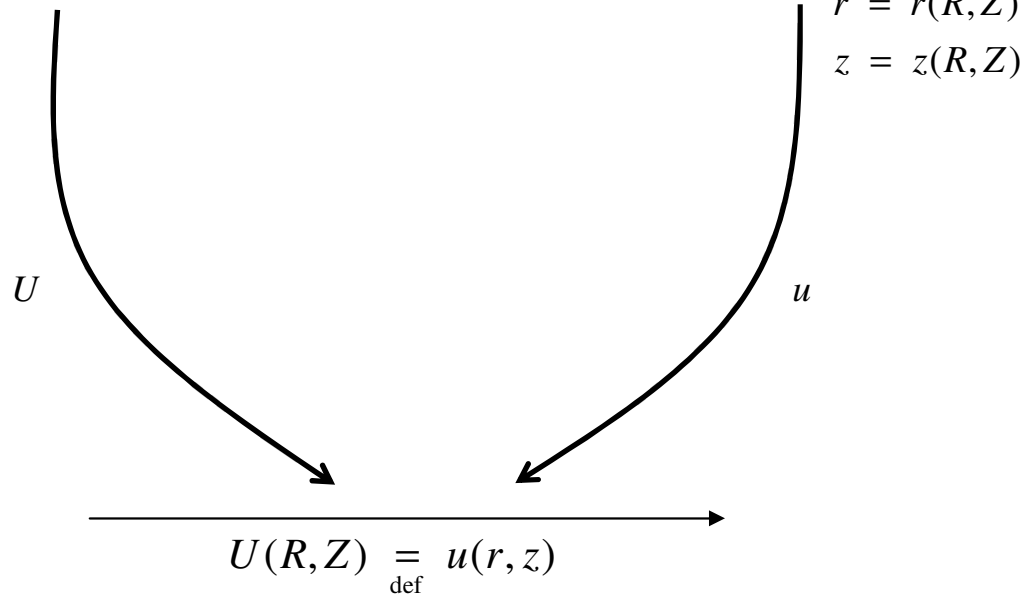
reference coordinates



space coordinates



(r, z)



physical equation for $u(r, z)$

→ partial diff'l equation (PDE) for $U(R, Z)$:

chain rule

$$\frac{\partial U}{\partial R} = \frac{\partial u}{\partial r} \frac{\partial r}{\partial R} + \frac{\partial u}{\partial z} \frac{\partial z}{\partial R}$$

$$\frac{\partial U}{\partial Z} = \frac{\partial u}{\partial r} \frac{\partial r}{\partial Z} + \frac{\partial u}{\partial z} \frac{\partial z}{\partial Z}$$

solve system of equations

$$\frac{\partial u}{\partial r} = \frac{1}{\Delta} \left(\frac{\partial U}{\partial R} \frac{\partial z}{\partial Z} - \frac{\partial U}{\partial Z} \frac{\partial z}{\partial R} \right)$$

$$\frac{\partial u}{\partial z} = \frac{1}{\Delta} \left(-\frac{\partial U}{\partial R} \frac{\partial r}{\partial Z} + \frac{\partial U}{\partial Z} \frac{\partial r}{\partial R} \right)$$

$$\text{with } \Delta = \frac{\partial r}{\partial R} \frac{\partial z}{\partial Z} - \frac{\partial r}{\partial Z} \frac{\partial z}{\partial R}$$

insert into PDE for u

Determine the functions $r(R, Z)$ and $z(R, Z)$

1. prescribed

a) physical deformation (e.g. structural mechanics)

b) explicit formula

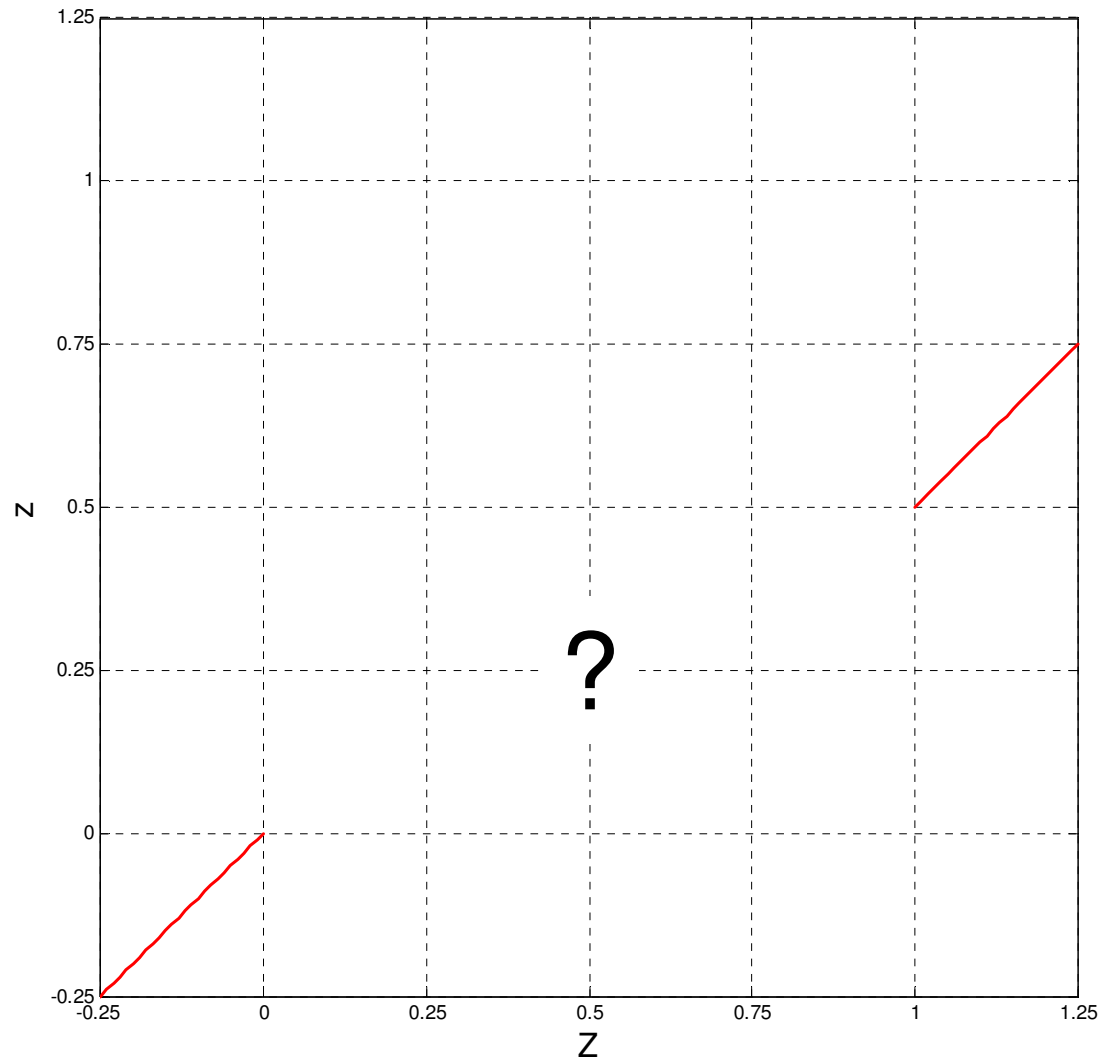
recommended here
(purely axial motion of rigid parts)

2. from boundary conditions

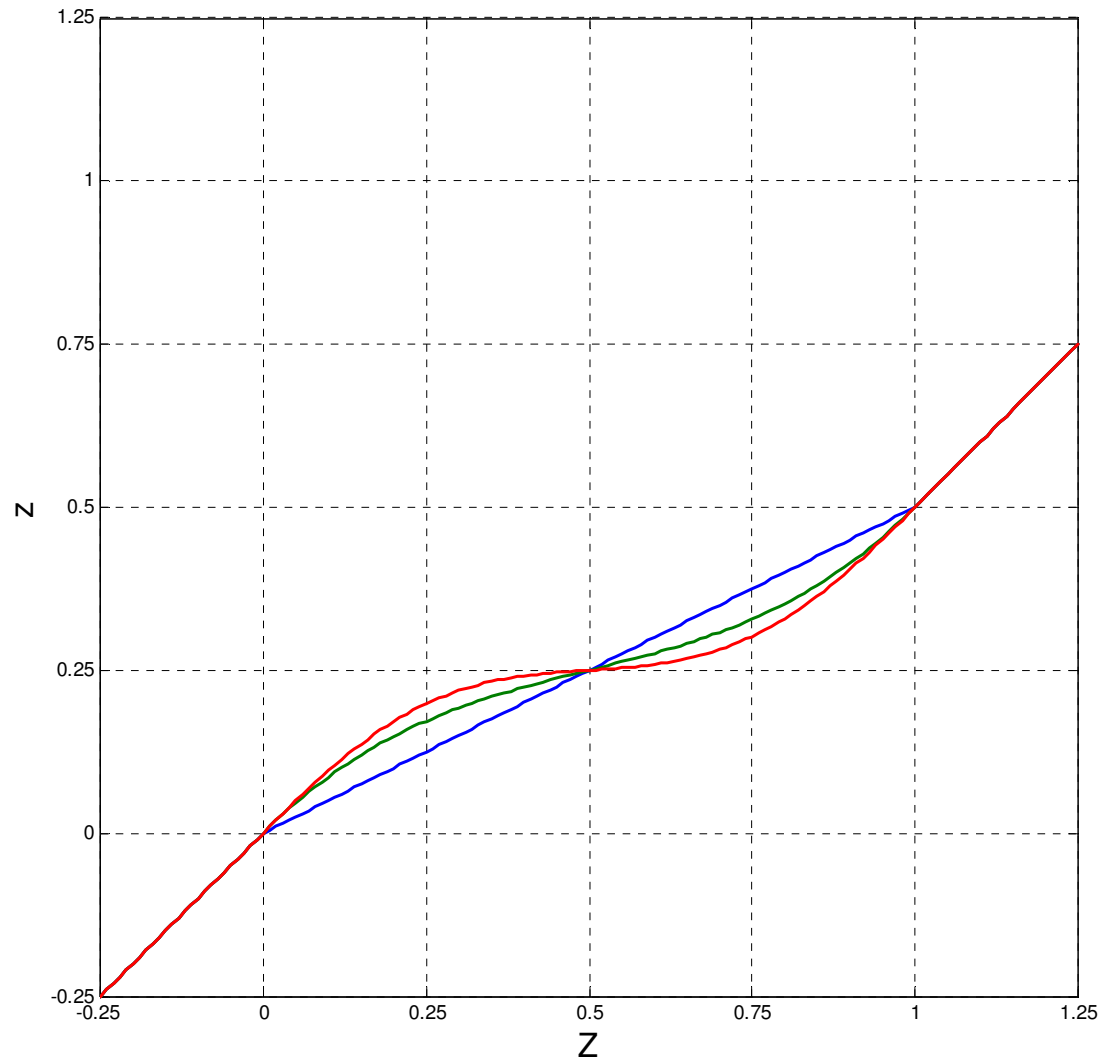
a) Laplace smoothing: $\frac{\partial^2 r}{\partial R^2} + \frac{\partial^2 z}{\partial Z^2} = 0$

b) Winslow smoothing: $\frac{\partial^2 R}{\partial r^2} + \frac{\partial^2 Z}{\partial z^2} = 0$

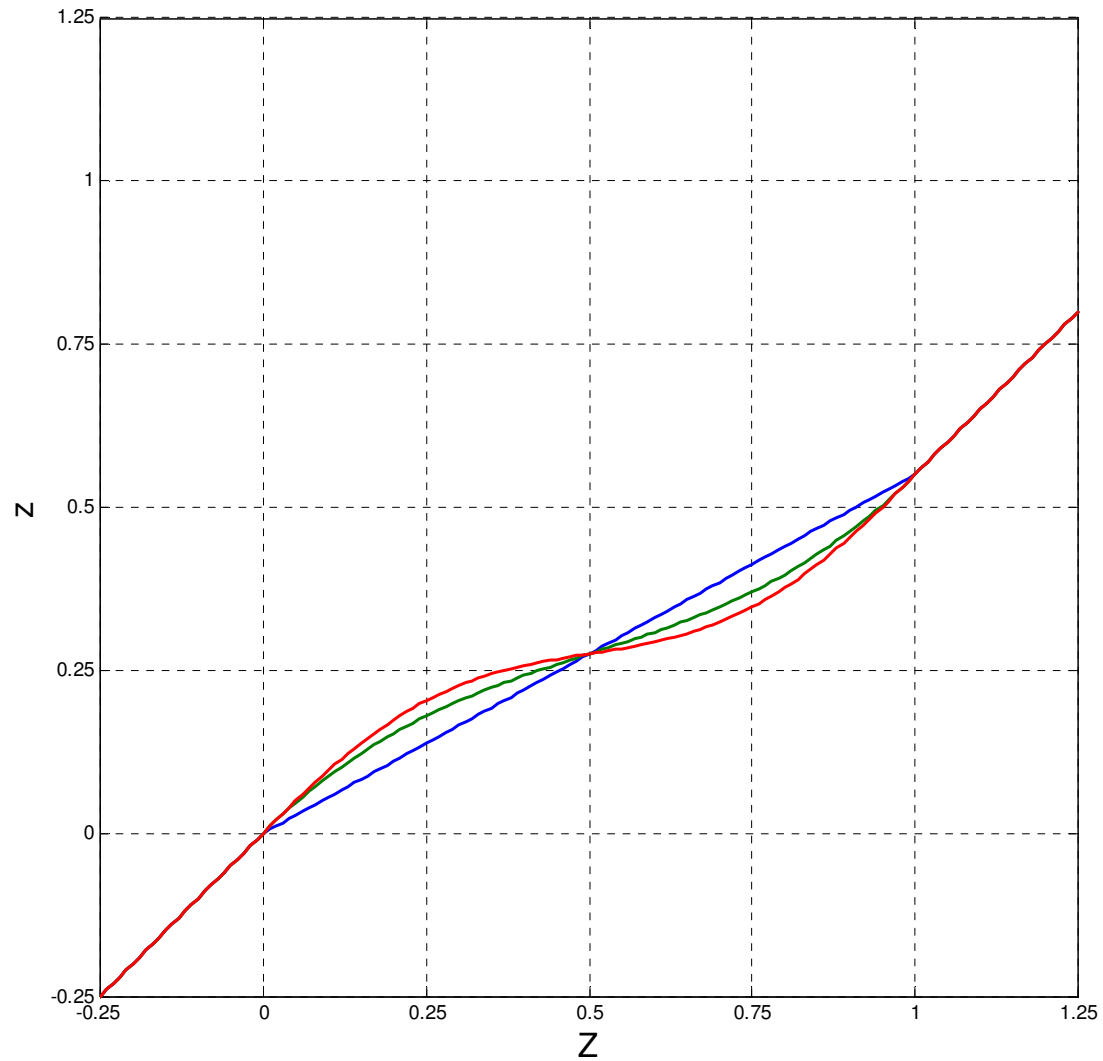
Explicit deformation $z(Z)$



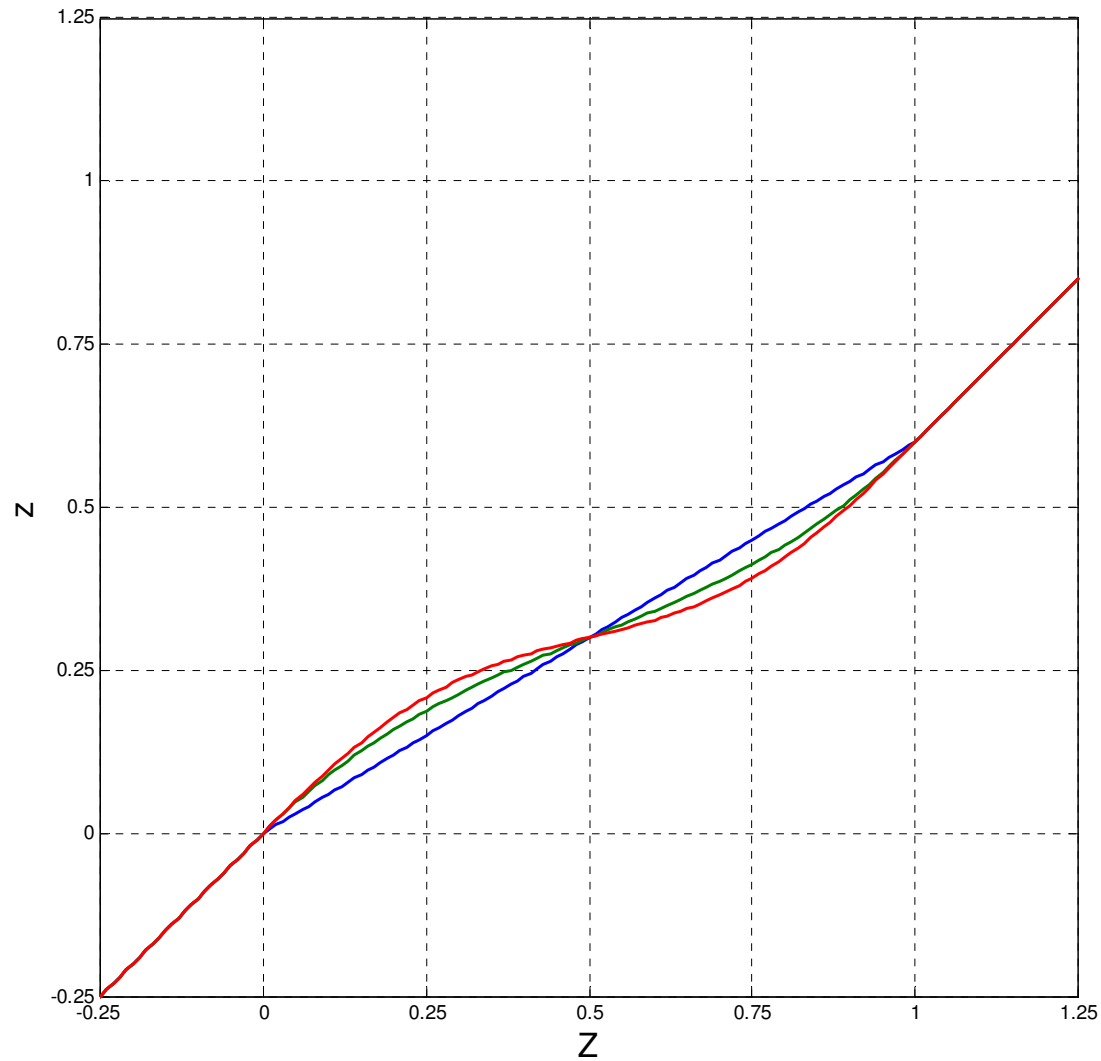
Continuous / differentiable deformations $z(Z)$



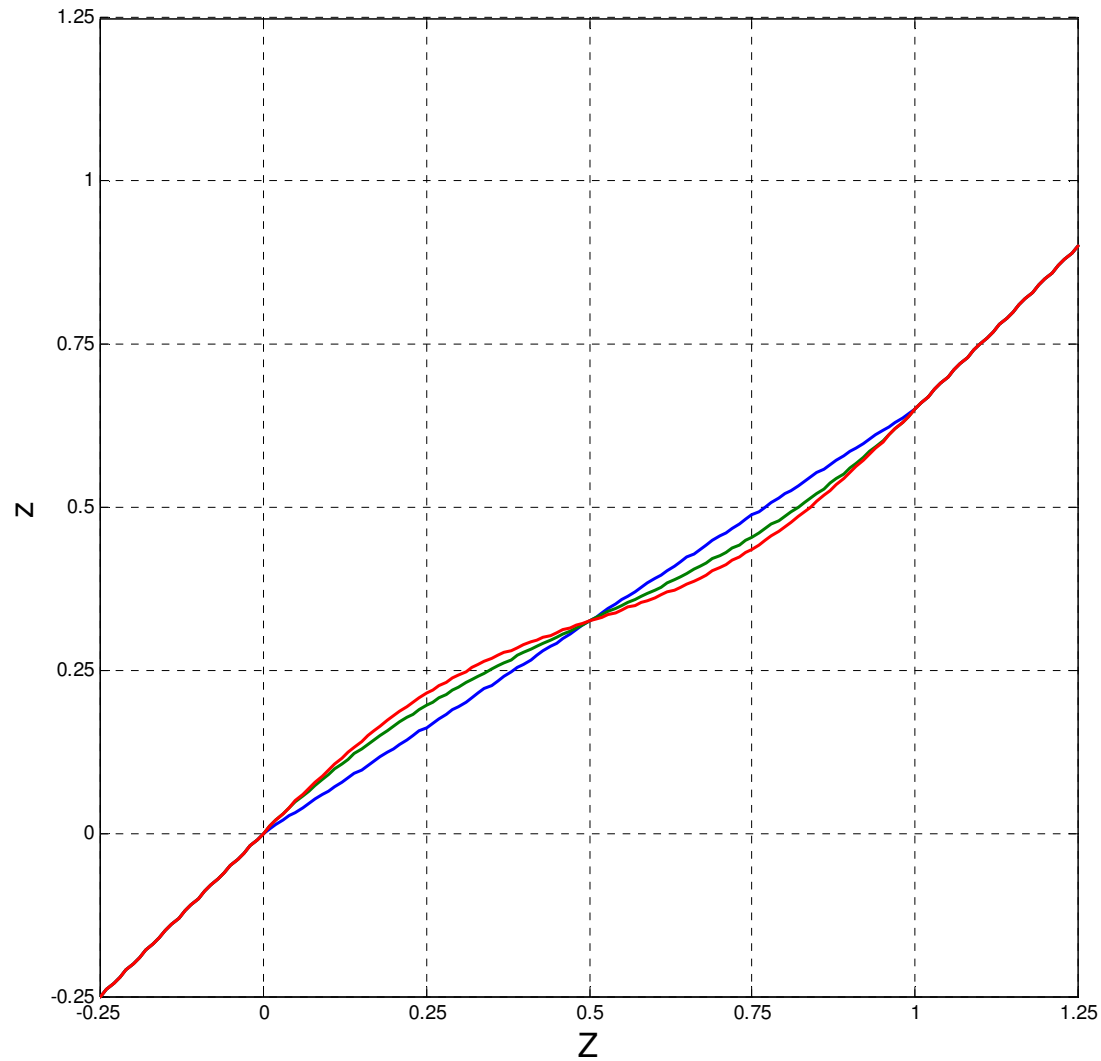
Continuous / differentiable deformations $z(Z)$



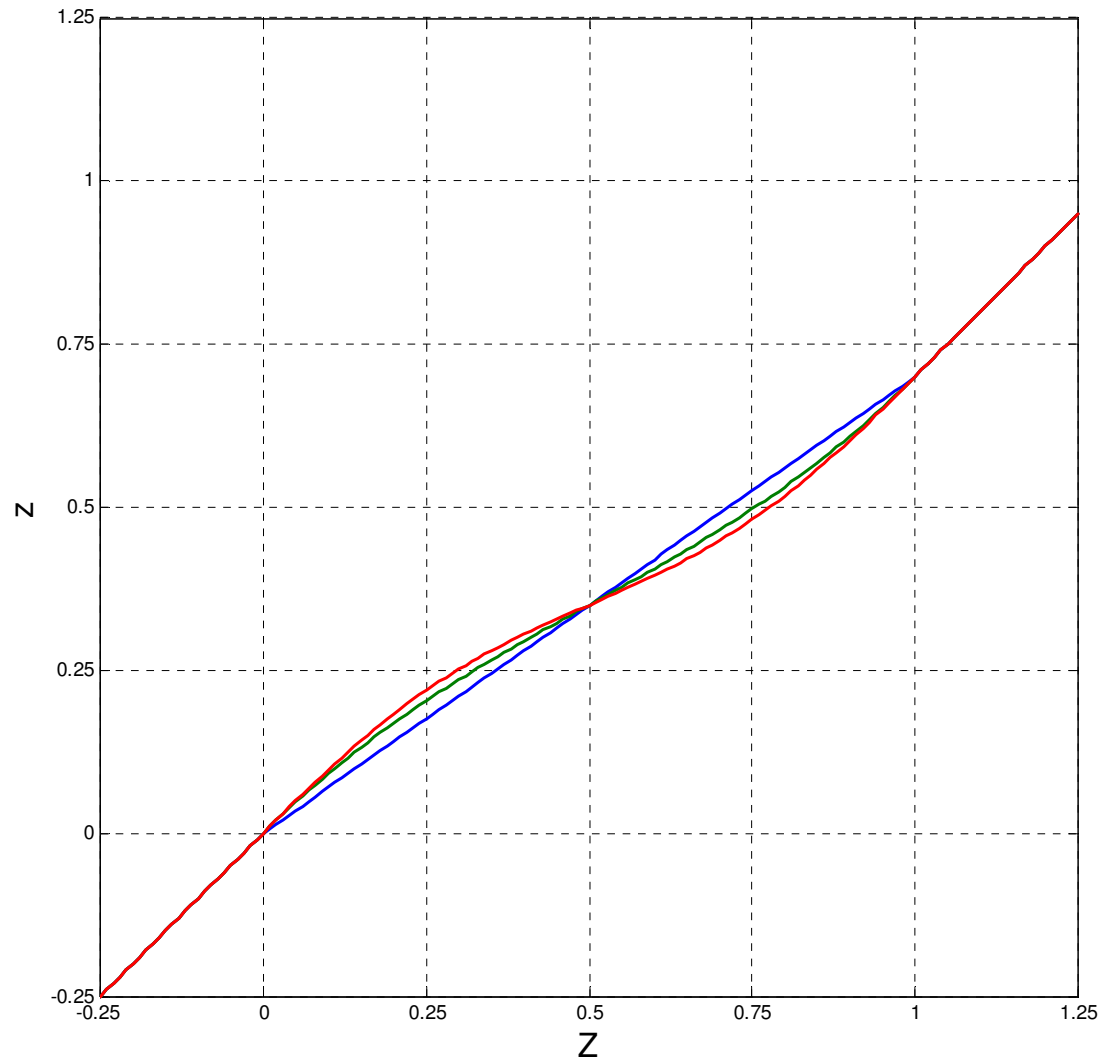
Continuous / differentiable deformations $z(Z)$



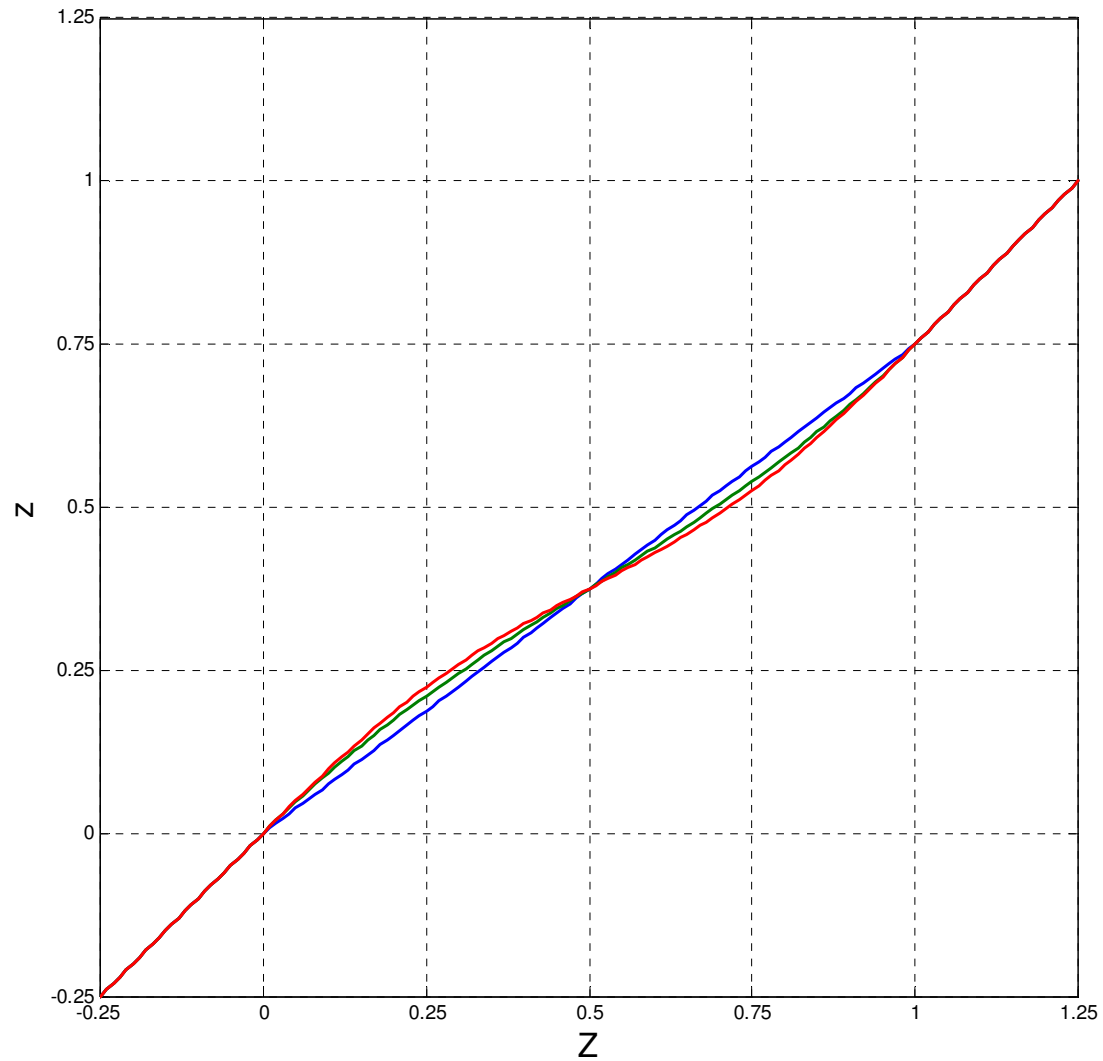
Continuous / differentiable deformations $z(Z)$



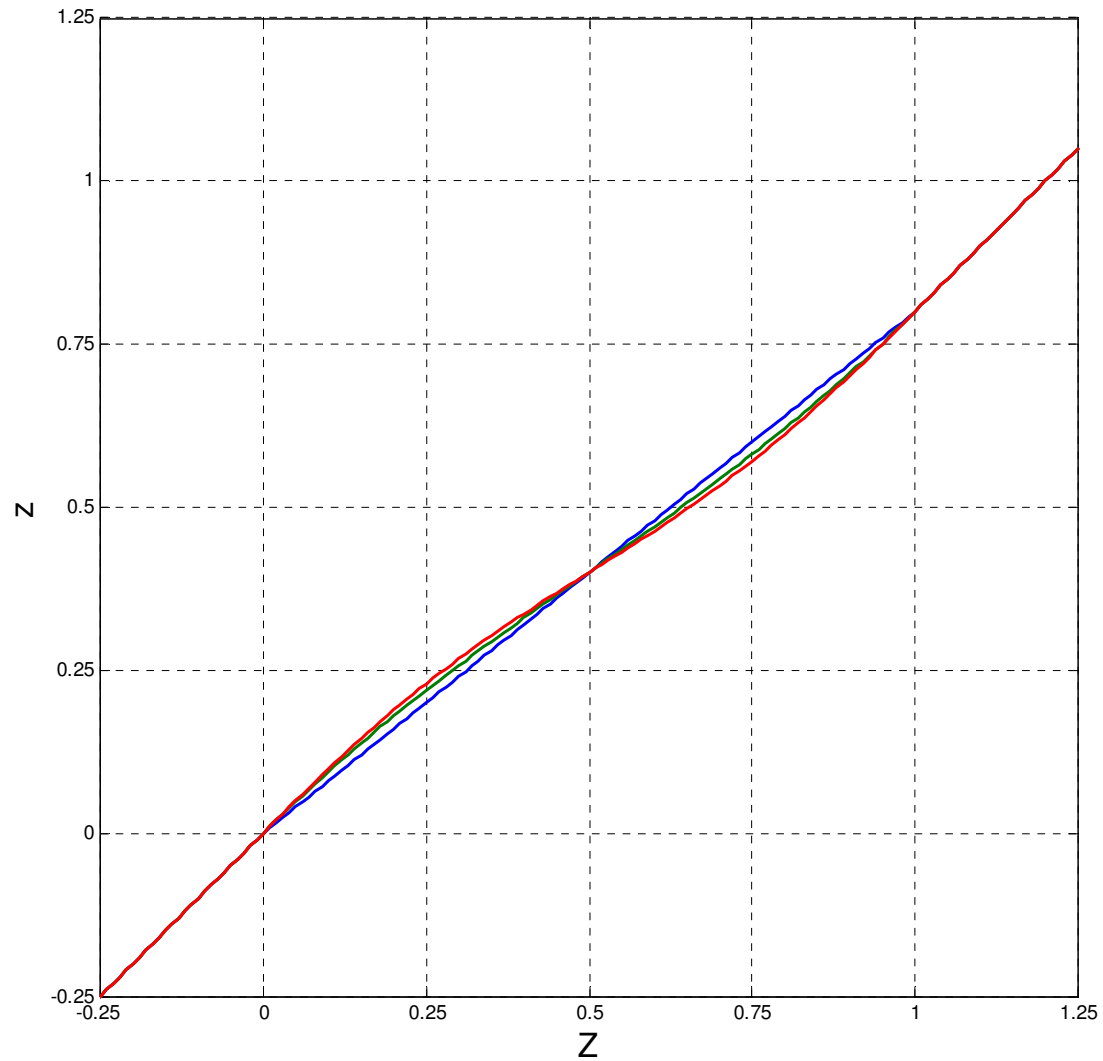
Continuous / differentiable deformations $z(Z)$



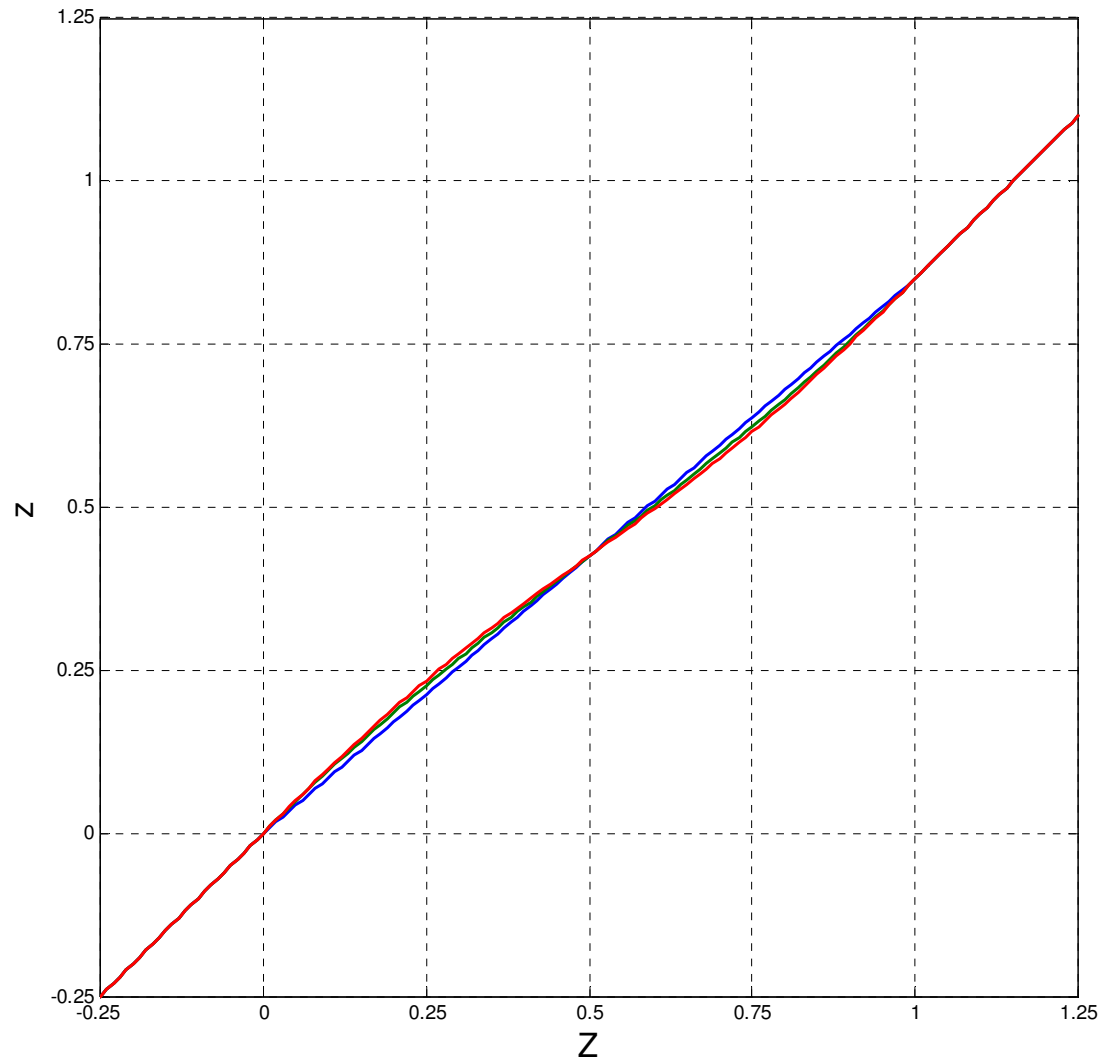
Continuous / differentiable deformations $z(Z)$



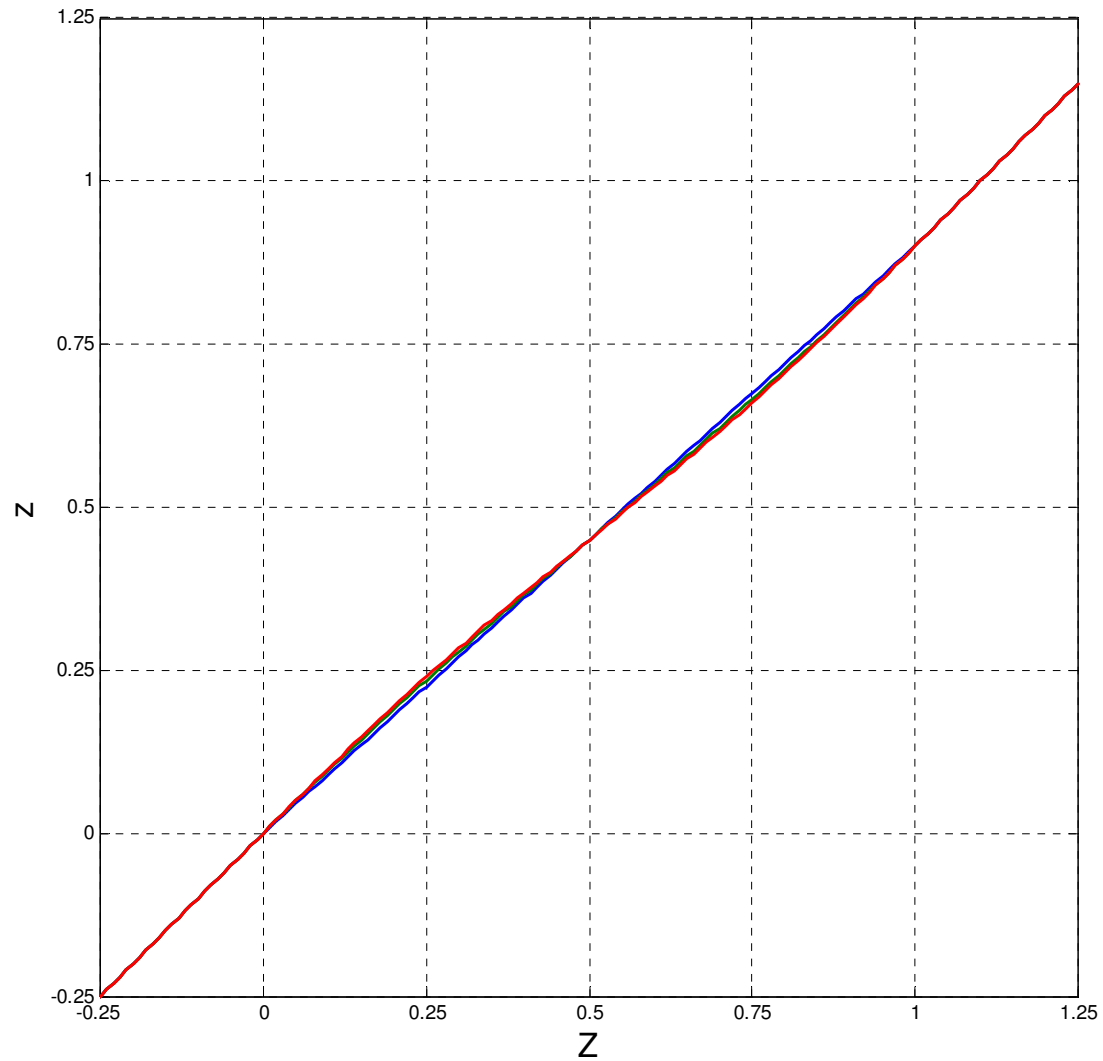
Continuous / differentiable deformations $z(Z)$



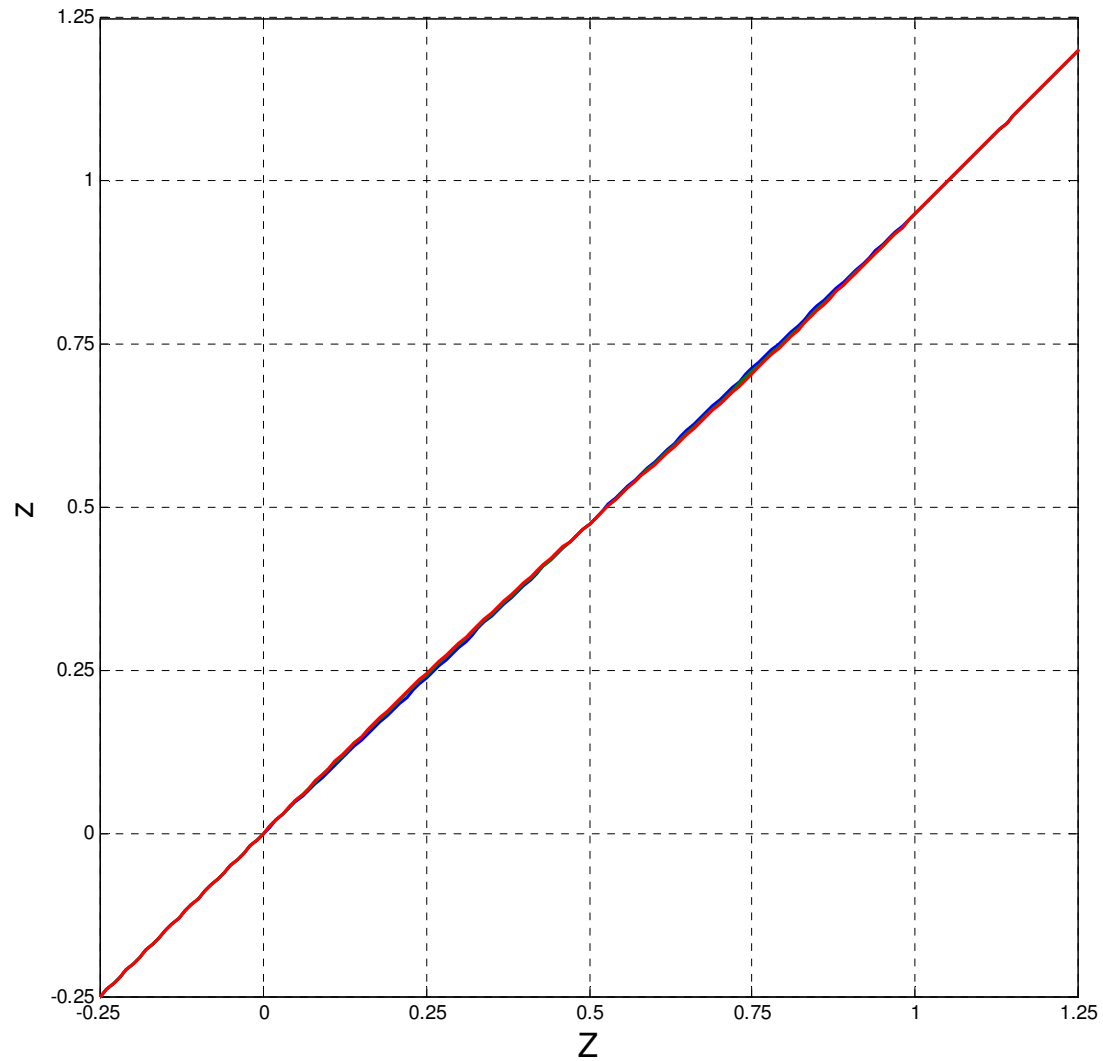
Continuous / differentiable deformations $z(Z)$



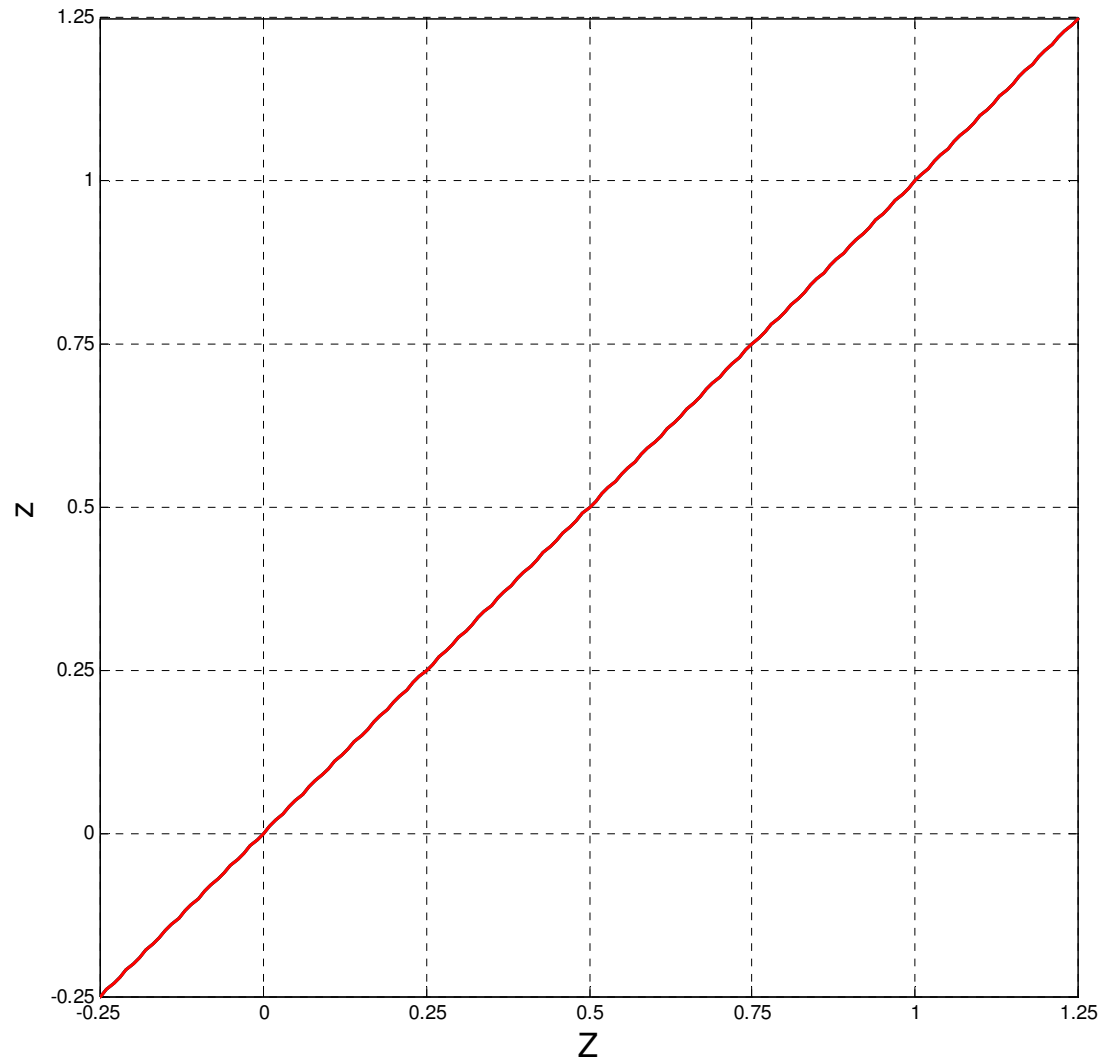
Continuous / differentiable deformations $z(Z)$



Continuous / differentiable deformations $z(Z)$

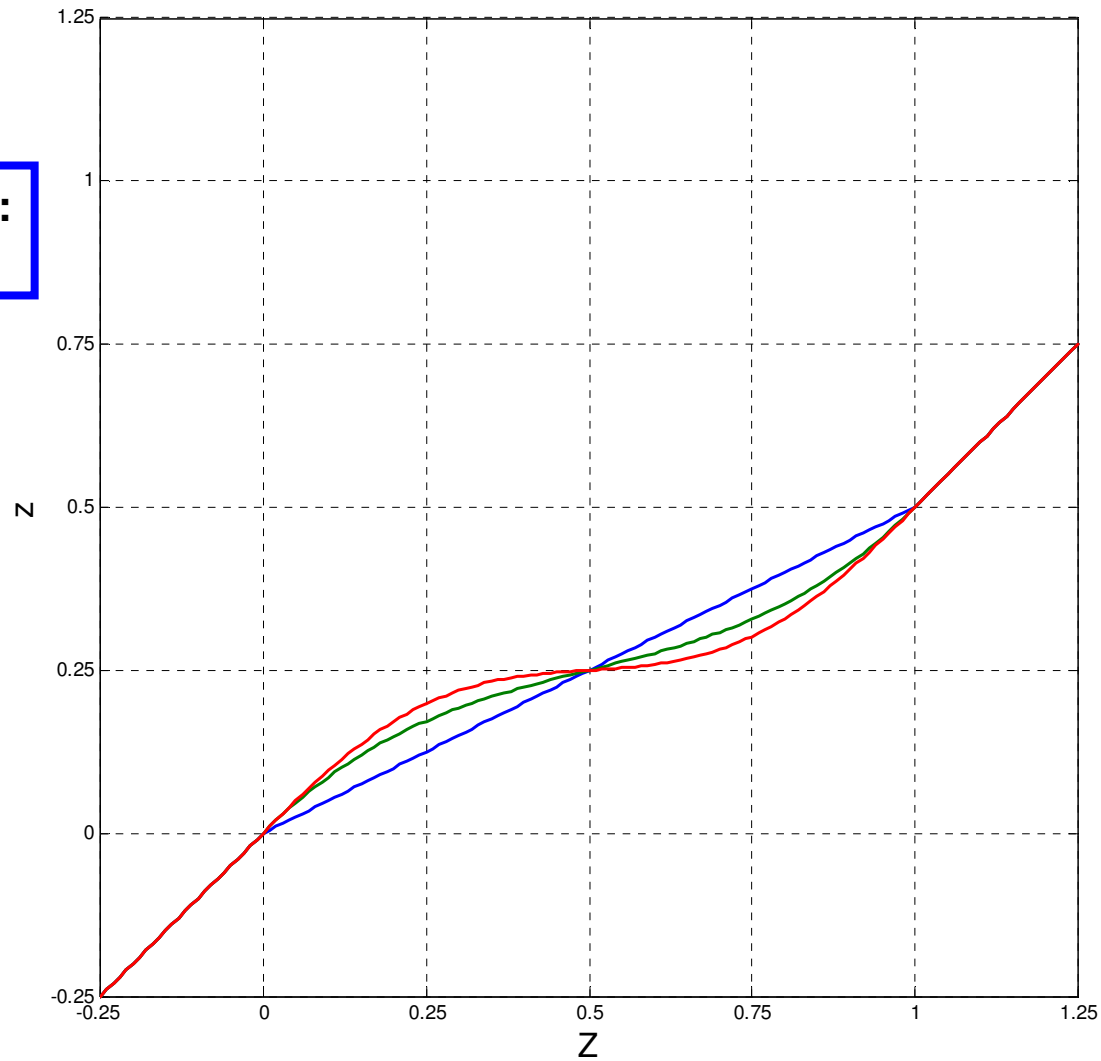


Continuous / differentiable deformations $z(Z)$



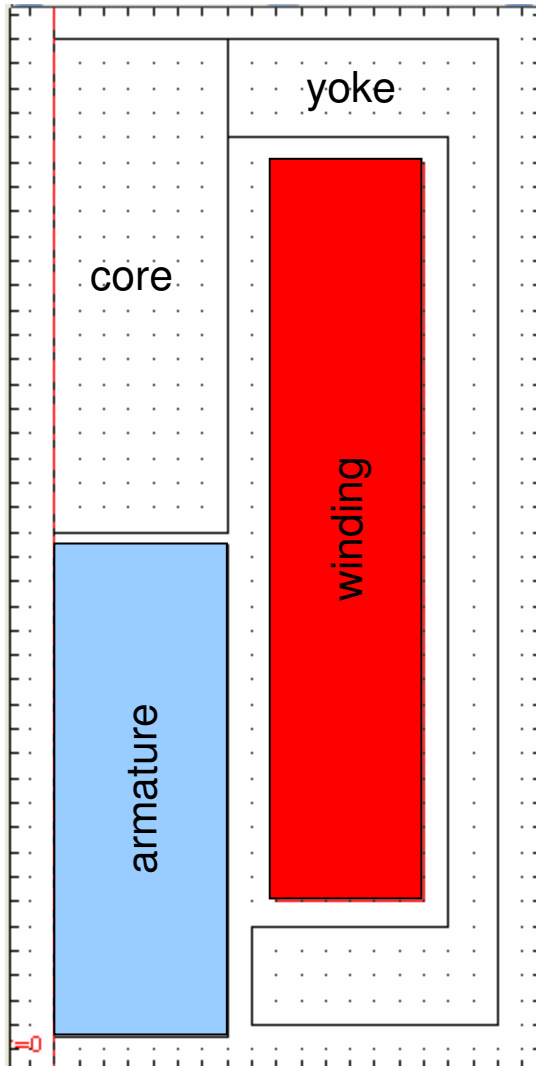
Continuous / differentiable deformations $z(Z)$

recommended here:
linear deformation

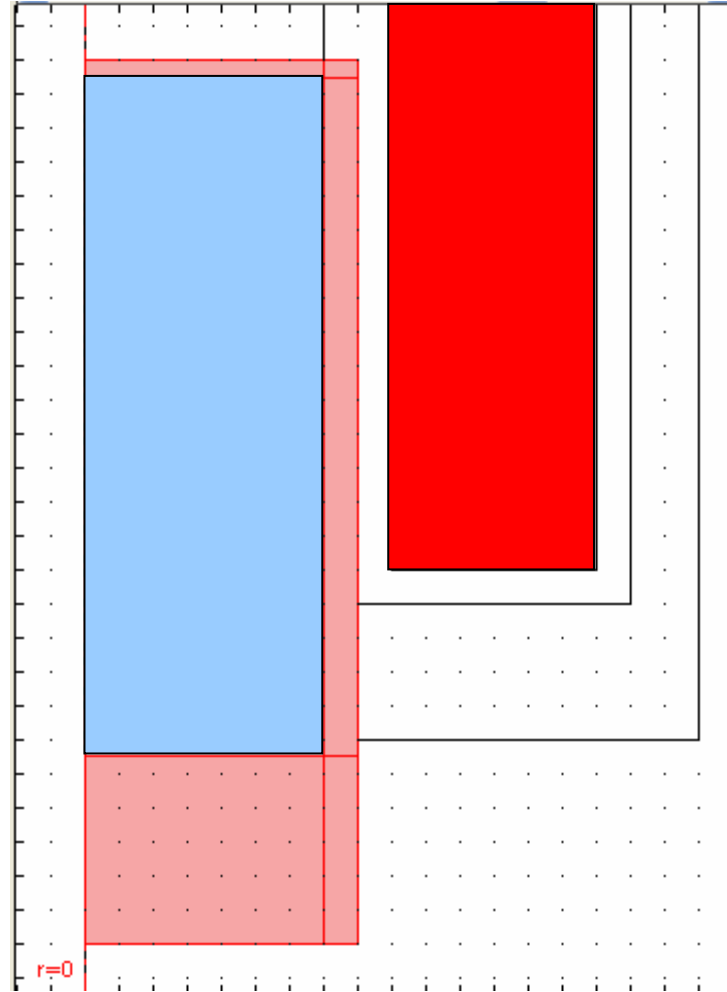


Geometry and deformation domain

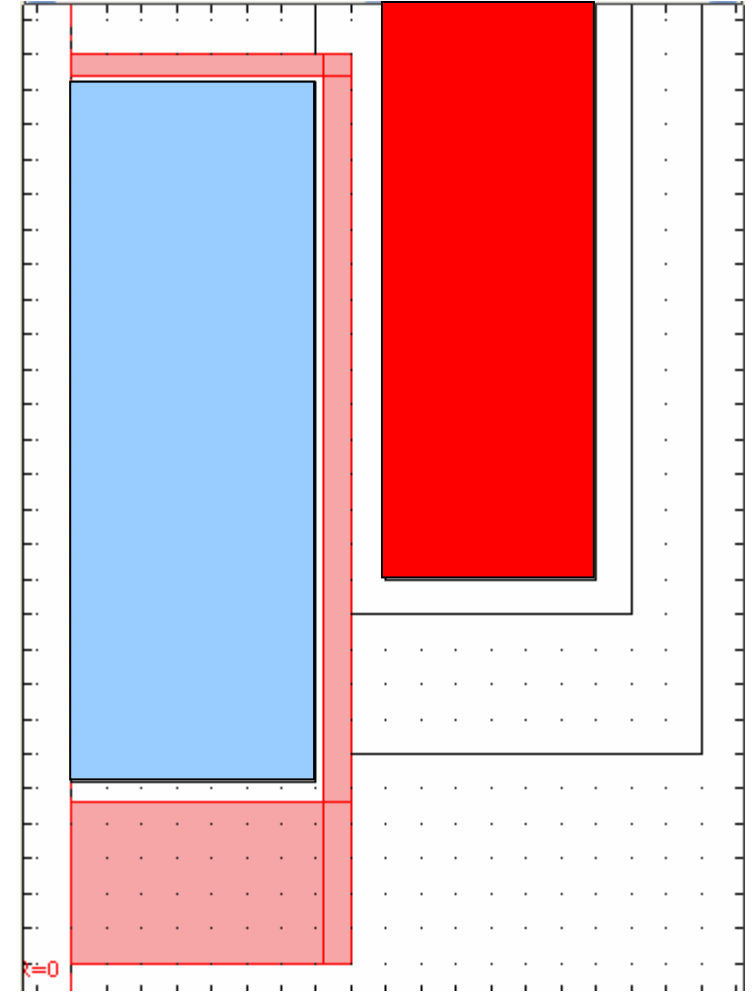
simplified geometry



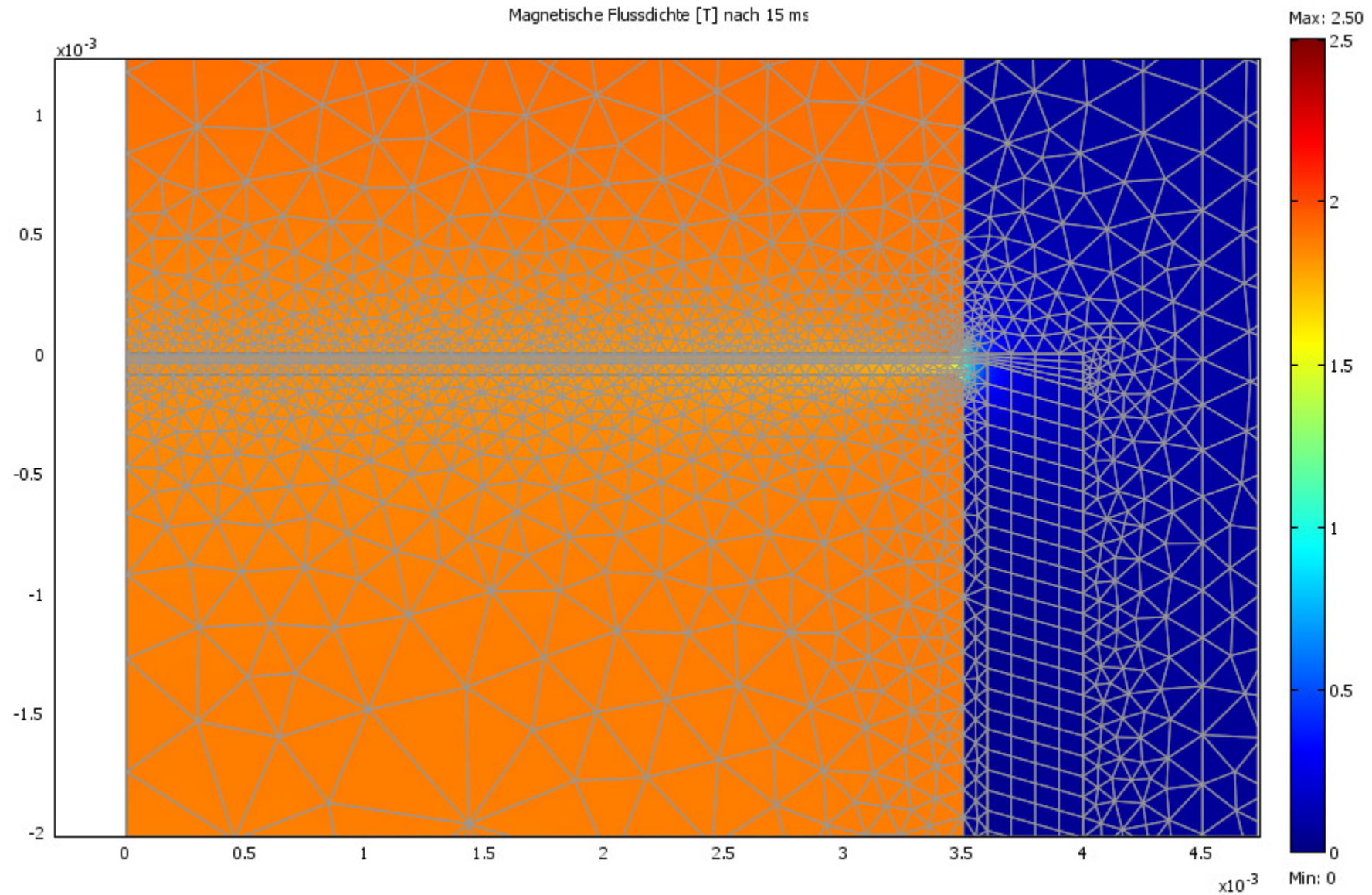
armature with deformation domain



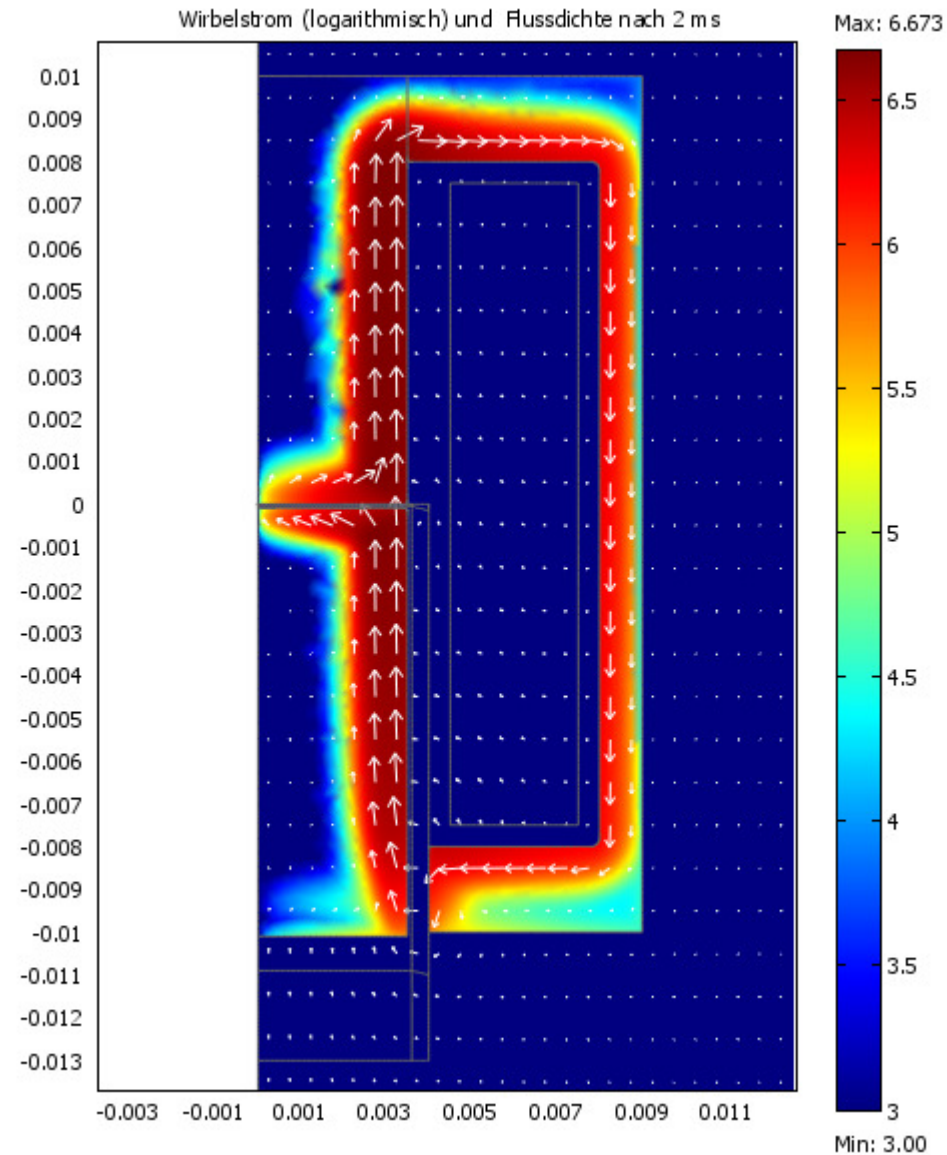
armature with rigid hull



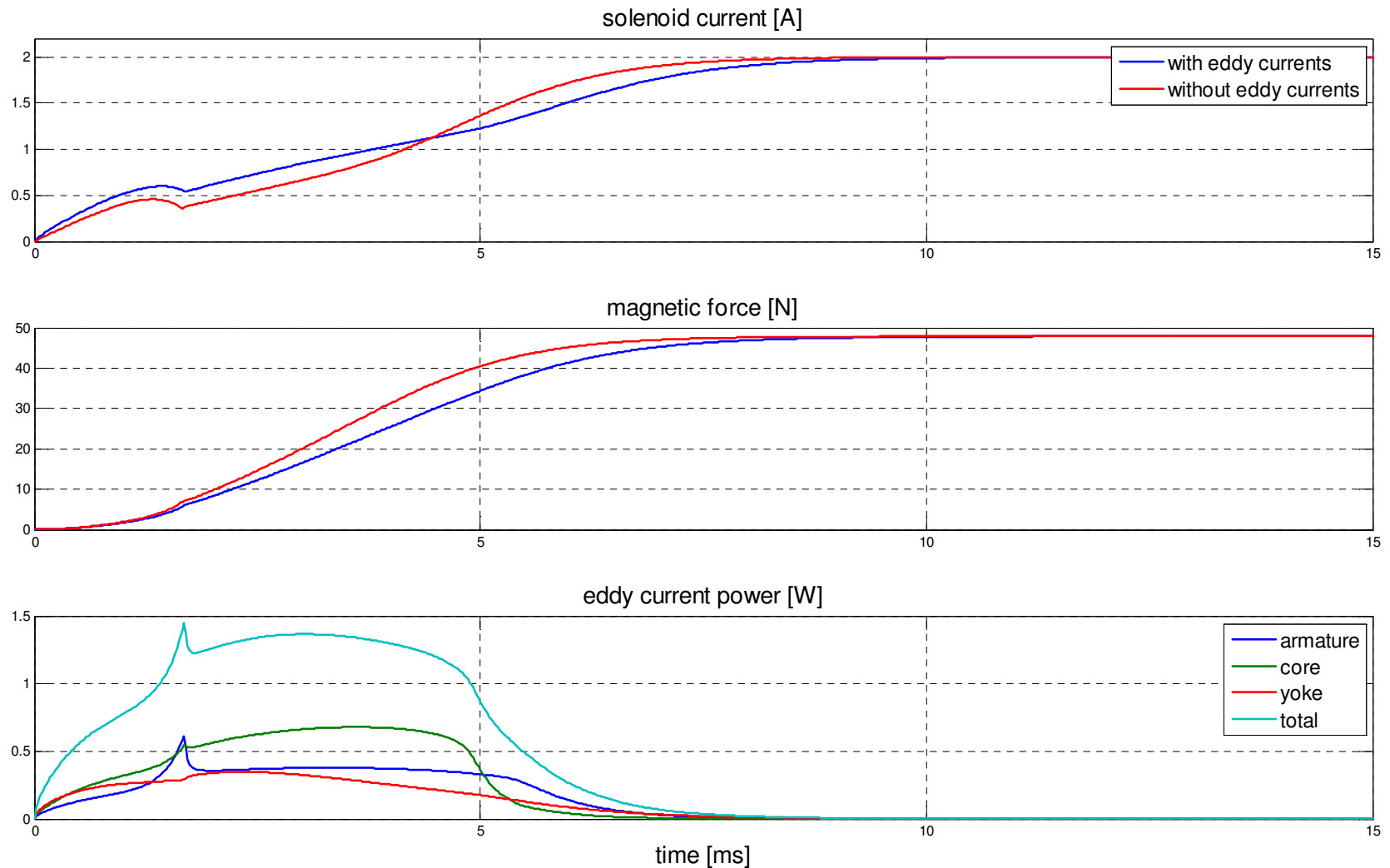
Voltage step response – mesh deformation and magnetic field



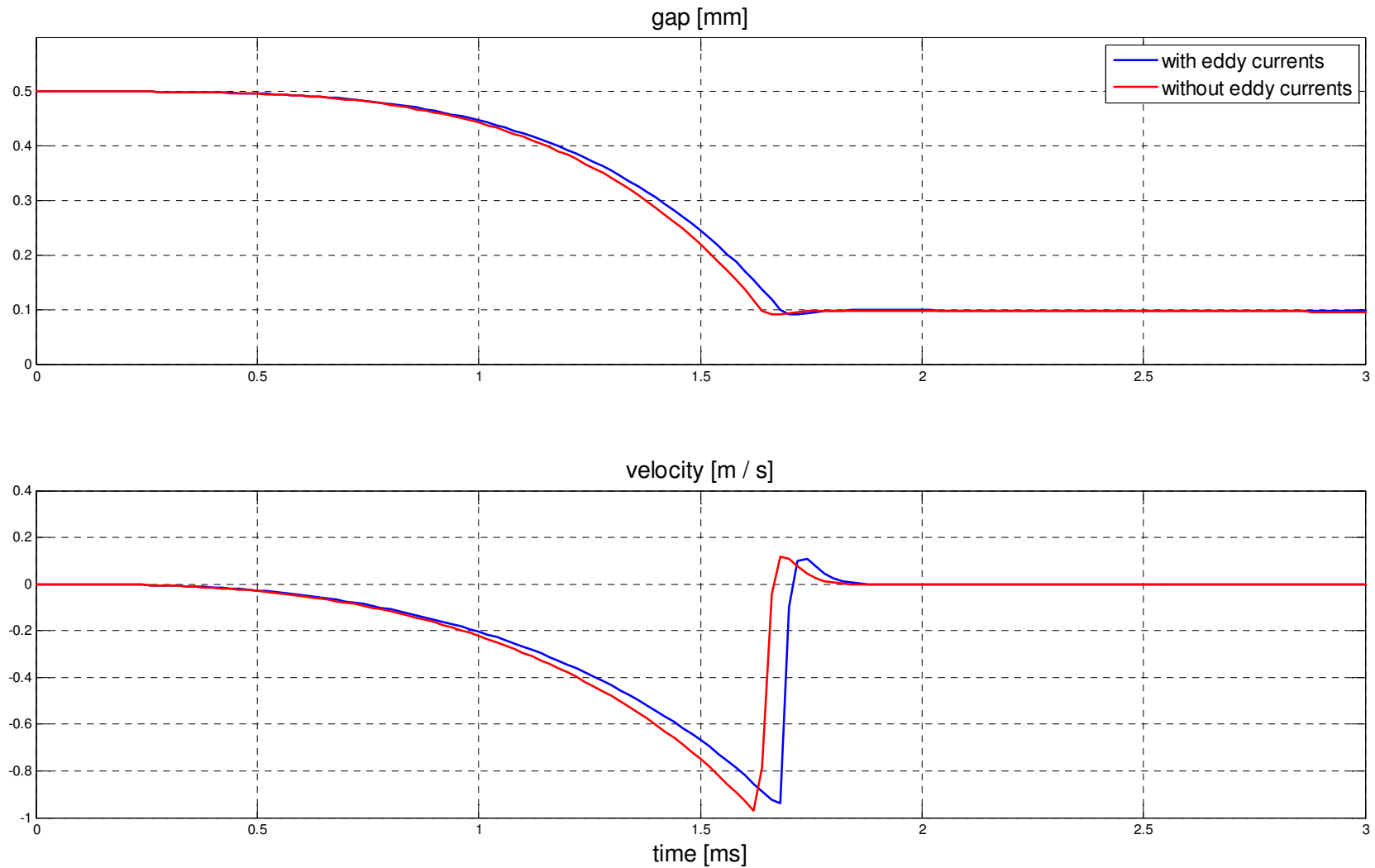
Voltage step response – eddy currents



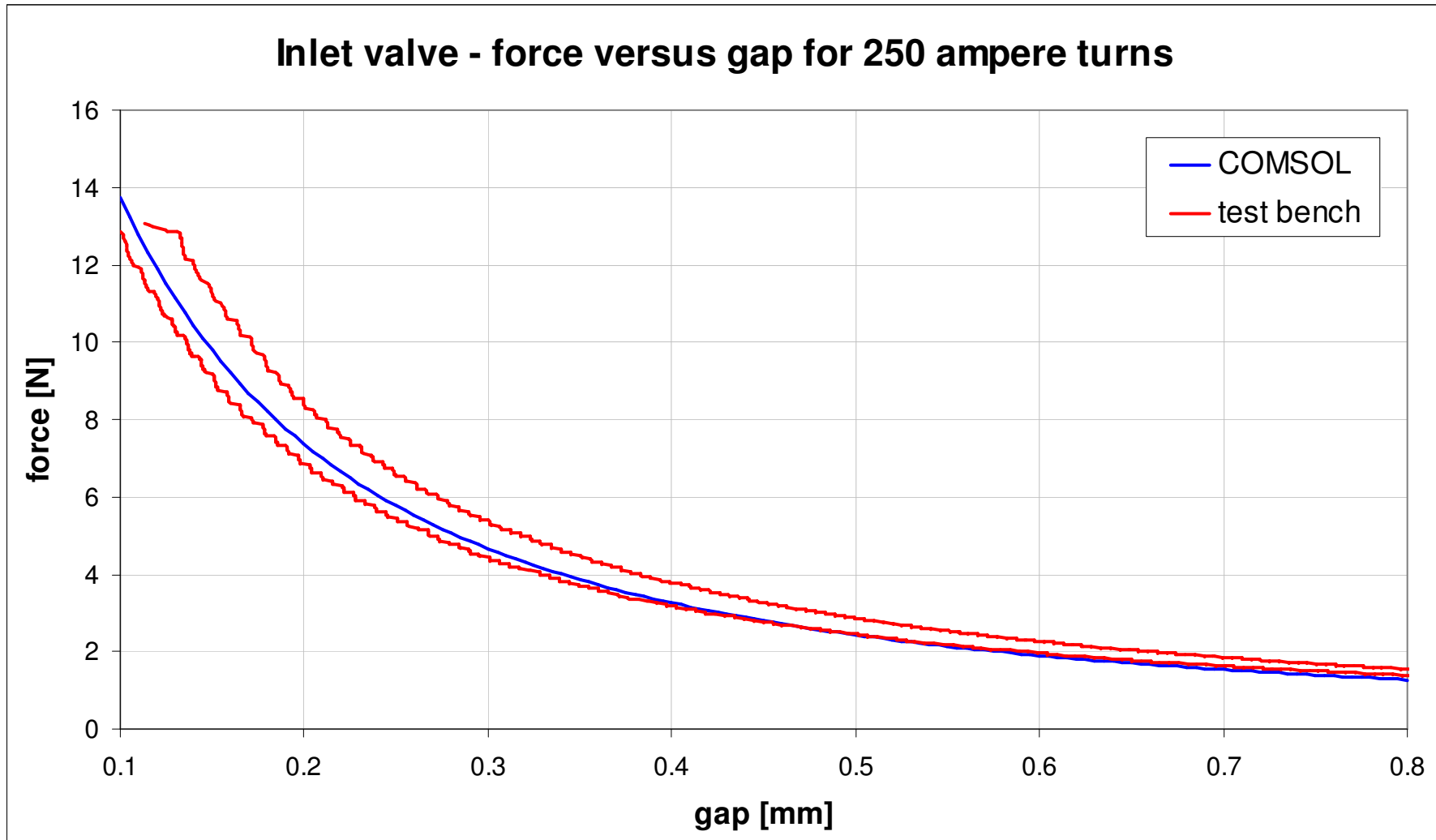
Voltage step response – armature motion



Voltage step response – armature motion



Comparison to experiment



Contents

1. Electronic brake systems by Continental Automotive Systems
 - ▶ ABS
 - ▶ ESC
2. COMSOL for electromagnetic actuators
 - ▶ Magnetic force
 - ▶ Armature movement by mesh deformation
 - ▶ Fast calculation of system dynamics
3. Conclusion

Static dependence of field on solenoid current (up to eddy currents)

$$\begin{aligned} \text{rot } \vec{H} = \vec{J} &= \sigma(\vec{E} + \vec{v} \times \vec{B}) + \vec{J}_{\text{ext}} \\ &= \sigma(\vec{E} + v \vec{e}_z \times \vec{B}) + \frac{n I_{\text{ext}} \vec{e}_\varphi}{S_{\text{coil}}} \\ -\sigma \vec{E} + \text{rot } \vec{H} - \sigma v \vec{e}_z \times \vec{B} &= \frac{n I_{\text{ext}} \vec{e}_\varphi}{S_{\text{coil}}} \end{aligned}$$

$$\mu_0 \mu_r \vec{H} = \vec{B} = \text{rot } \vec{A}$$

$$\vec{E} = -\frac{\partial \vec{A}}{\partial t}$$

0 (neglect eddy currents from field change)

$$\sigma \frac{\partial \vec{A}}{\partial t} + \text{rot} \left(\frac{1}{\mu_0 \mu_r} \text{rot } \vec{A} \right) - \sigma v \vec{e}_z \times \text{rot } \vec{A} = \frac{n I_{\text{ext}} \vec{e}_\varphi}{S_{\text{coil}}}$$

$$\vec{A} = \vec{A}(I_{\text{ext}}, v, x)$$

Dynamics of solenoid current: integral parameter magnetic flux

$$\begin{aligned} I_{\text{ext}} &= \frac{1}{R} (U_{\text{ext}} + U_{\text{ind}}) \\ &= \frac{1}{R} \left(U_{\text{ext}} + \frac{n}{S_{\text{coil}}} \iint_{S_{\text{coil}}} 2 \pi r \vec{E} \, dr \, dz \right) \\ &= \frac{1}{R} \left(U_{\text{ext}} - \frac{d}{dt} \underbrace{\left(\frac{n}{S_{\text{coil}}} \iint_{S_{\text{coil}}} 2 \pi r \vec{A} \, dr \, dz \right)}_{\Psi} \right) \end{aligned}$$

$$I_{\text{ext}} = \frac{1}{R} \left(U_{\text{ext}} - \frac{d\Psi}{dt} \right), \quad \Psi = \Psi(\vec{A}) = \Psi(\vec{A}(I_{\text{ext}}, v, x))$$

System dynamics

$$I_{\text{ext}} = \frac{1}{R} \left(U_{\text{ext}} - \frac{d\Psi}{dt} \right),$$

$$\Psi = \Psi(I_{\text{ext}}, v, x)$$



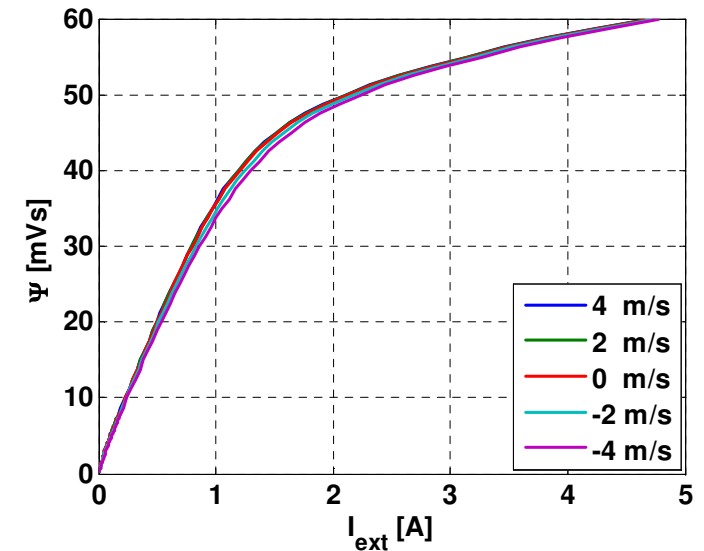
$$I_{\text{ext}} = I_{\text{ext}}(\Psi, v, x)$$

- COMSOL solves $\Psi(I_{\text{ext}}) = \Psi_{\text{prescr}}$ for I_{ext}
- look-up table / interpolation

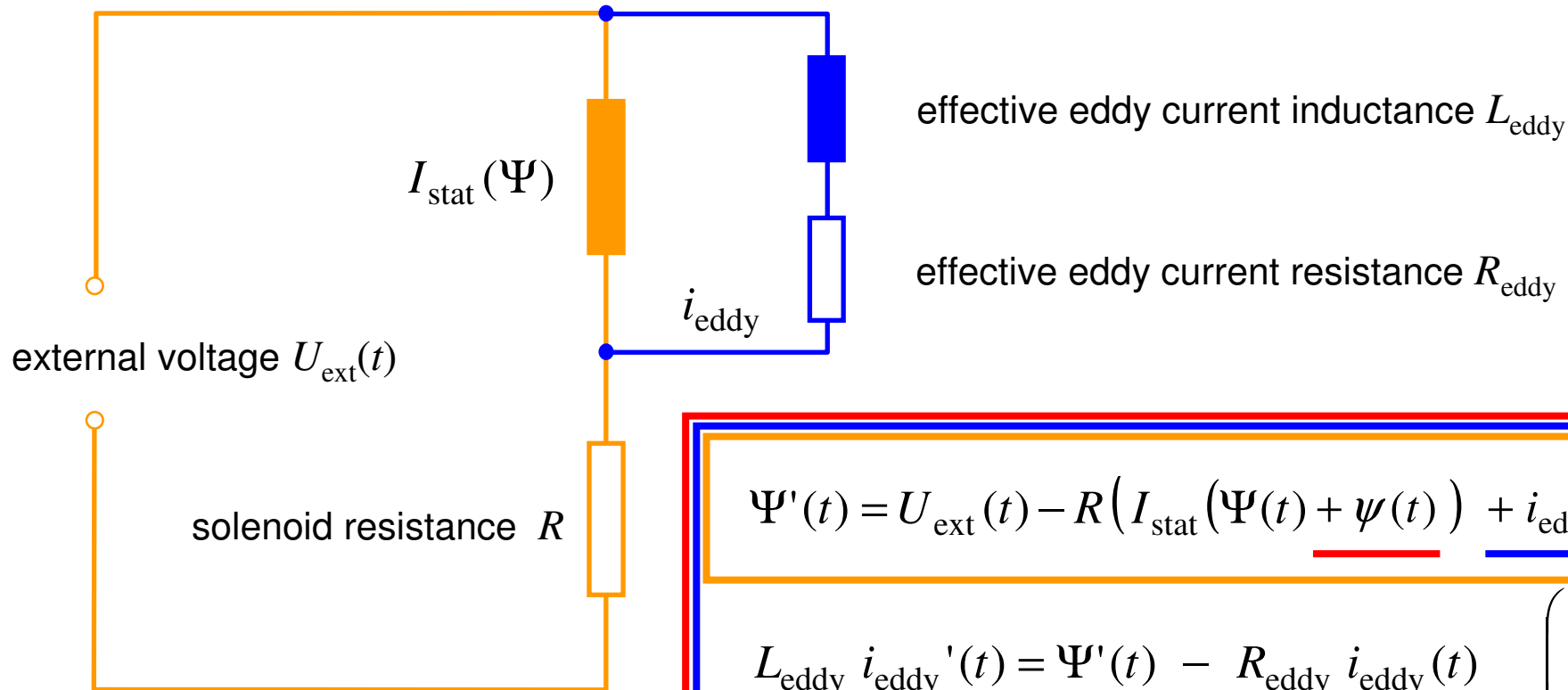
$$\frac{d\Psi}{dt} = U_{\text{ext}} - R \cdot I_{\text{ext}}(\Psi, v, x)$$

+ armature equation of motion

+ simple effective eddy current model



Effective eddy current model



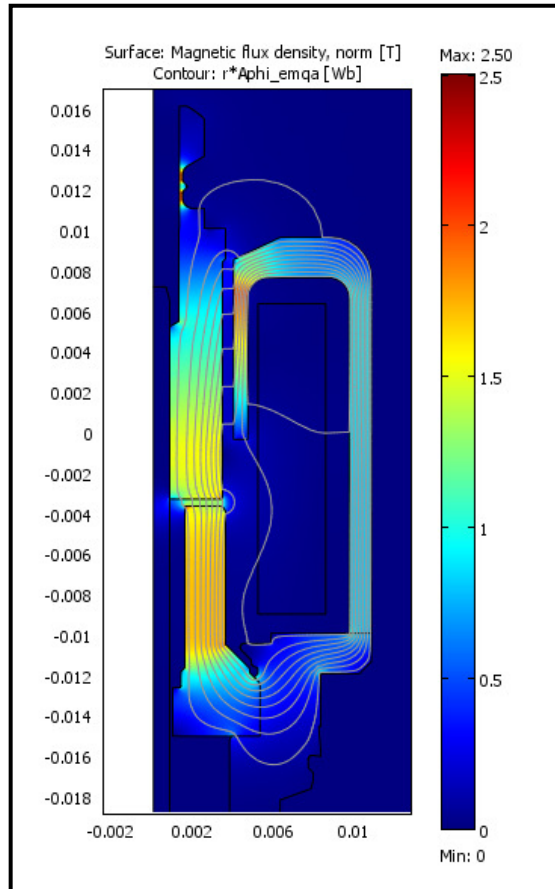
$$\Psi'(t) = U_{\text{ext}}(t) - R \left(\underline{I_{\text{stat}}(\Psi(t) + \psi(t))} + \underline{i_{\text{eddy}}(t)} \right)$$

$$L_{\text{eddy}} i_{\text{eddy}}'(t) = \Psi'(t) - R_{\text{eddy}} i_{\text{eddy}}(t) \quad \left(\frac{L_{\text{eddy}}}{R_{\text{eddy}}} \approx 1 \text{ ms} \right)$$

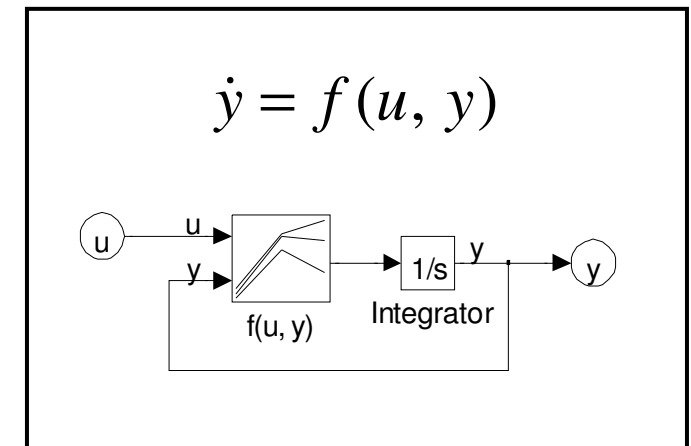
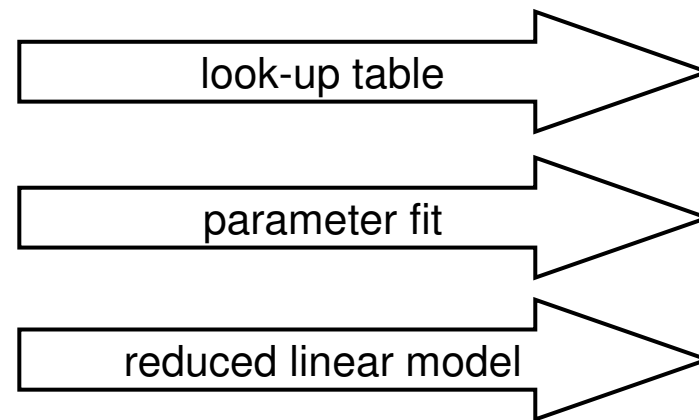
$$\tau_1 \psi'(t) = \tau_2 \Psi'(t) - \psi(t) \quad (\tau_1 \approx 0.02 \text{ ms})$$

determine $L_{\text{eddy}}, R_{\text{eddy}}, \tau_1, \tau_2$ from least squares fit to Comsol result

Generation of small systems of ordinary differential equations



field problem
(e.g. COMSOL)



dynamic system
(e.g. Simulink)

- fast solution
- parameter variation
- integration into comprehensive model

Conclusion – simulation in industrial development

1. efficiency

- ▶ fewer prototypes
- ▶ better experiments

2. product performance

- ▶ more variants
- ▶ automatic optimization
- ▶ functional insight
 - “observe” new quantities
 - isolate parameter influence

3. robust products

- ▶ create limit configurations
- ▶ study tolerances statistically