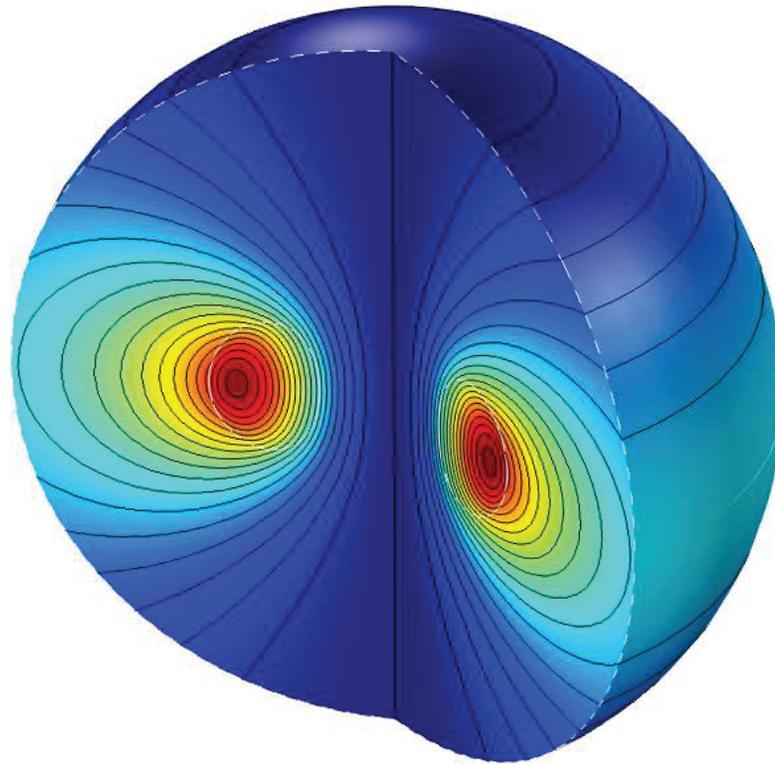


# STRUCTURE OF A CLASSICAL VORTEX RING

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# OBJECTIVE

Develop a COMSOL simulation that incorporates complications such as those shown here:

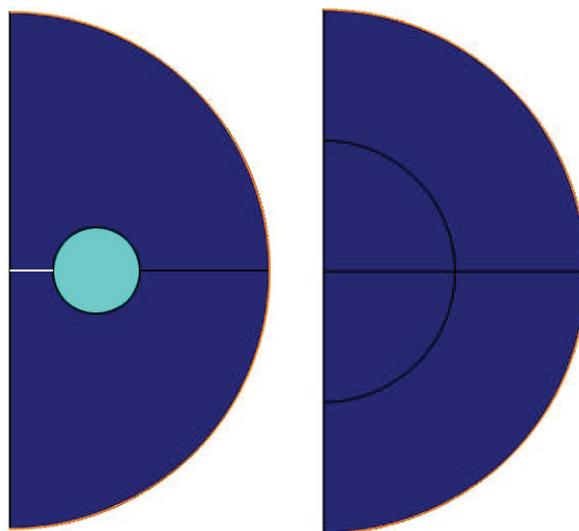


# SPHERICAL COORDINATES IN PHYSICAL AND PROXY DOMAINS VIA KELVIN INVERSION

	Physical domain	Conver- sion	Proxy domain
Radial	$R$	$Rq = a^2$	$q$
Colatitudinal	$\theta$	$\theta = \vartheta$	$\vartheta$
Azimuthal	$\phi$	$\phi = \varphi$	$\varphi$

$$R \frac{\partial}{\partial R} = -q \frac{\partial}{\partial q} \quad , \quad \frac{\partial}{\partial \theta} = \frac{\partial}{\partial \vartheta} \quad , \quad \frac{\partial}{\partial \phi} = \frac{\partial}{\partial \varphi}$$

$$\hat{\mathbf{e}}_R = \hat{\mathbf{u}}_q \quad , \quad \hat{\mathbf{e}}_\theta = \hat{\mathbf{u}}_\vartheta \quad , \quad \hat{\mathbf{e}}_\phi = \hat{\mathbf{u}}_\varphi$$



**Figure 1** Schematic views of meridional sections of  $\mathcal{R}^i$  (left panel) and  $\mathcal{Q}$  (right panel). In the left panel the light blue region is a section of  $\mathcal{R}^c$  and the dark blue region is a section of  $\mathcal{R}^i \setminus \mathcal{R}^c$ . The short white segment there is a section of the diaphragm,  $\mathcal{S}^d$ .

# CYLINDRICAL COORDINATES IN PHYSICAL AND PROXY DOMAINS VIA KELVIN INVERSION

Physical  
domain

Proxy  
domain

Transverse	$r = R \sin \theta$	$\varpi = q \sin \vartheta$
Axial	$z = R \cos \theta$	$\zeta = q \cos \vartheta$

$$\hat{\mathbf{e}}_r = \hat{\mathbf{u}}_\varpi \quad , \quad \hat{\mathbf{k}} = \hat{\mathbf{u}}_\zeta$$

Meridional gradient operators:

$$\nabla^{(m)} := \hat{\mathbf{e}}_r \frac{\partial}{\partial r} + \hat{\mathbf{k}} \frac{\partial}{\partial z} \quad , \quad \nabla_q^{(m)} := \hat{\mathbf{u}}_\varpi \frac{\partial}{\partial \varpi} + \hat{\mathbf{u}}_\zeta \frac{\partial}{\partial \zeta}$$

# FIELD EQUATIONS IN THREE DOMAINS

In the vortex core,  $\mathcal{R}^c$ :

$$\nabla^{(m)} \cdot [(1/r) \nabla^{(m)} \Psi] = Ar ,$$

in which the velocity components  $(u_r, u_z)$  satisfy  $u_r = (1/r) \partial \Psi / \partial z$ ,  $u_z = -(1/r) \partial \Psi / \partial r$  and  $A$  is a constant. In the bounded region of irrotational motion,  $\mathcal{R}^i \setminus \mathcal{R}^c$ :

$$\nabla^{(m)} \cdot (r \nabla^{(m)} \Phi) = 0 ,$$

in which  $u_r = \partial \Phi / \partial r$ ,  $u_z = \partial \Phi / \partial r$ . In the proxy exterior,  $\mathcal{Q}$ :

$$\nabla_q^{(m)} \cdot [\varpi (a^2 / q^2) \nabla_q^{(m)} \Phi] = 0 .$$

## CONDITIONS ON THE PORTAL

Let  $\partial(\mathcal{R}^i \setminus \mathcal{R}^c)_>$  be the outer boundary of  $\mathcal{R}^i \setminus \mathcal{R}^c$  and think of  $\partial(\mathcal{R}^i \setminus \mathcal{R}^c)_>$  and  $\partial\mathcal{Q}$  as two sides of a *portal*. Condition 1 there is a DIRICHLET condition for  $\Phi$  on  $\partial\mathcal{Q}$ , which equates it to the value of  $\Phi$  on  $\partial(\mathcal{R}^i \setminus \mathcal{R}^c)_>$ . Condition 2 there is a Flux/Source boundary condition for  $\Phi$  on  $\partial(\mathcal{R}^i \setminus \mathcal{R}^c)_>$ , namely

$$-\hat{\mathbf{n}} \cdot (r \nabla^{(m)} \Phi) = \frac{\varpi}{q} \left( \varpi \frac{\partial \Phi}{\partial \varpi} + \zeta \frac{\partial \Phi}{\partial \zeta} \right),$$

whose right member is the value of the left member after Kelvin Inversion and evaluation on  $\partial\mathcal{Q}$ .

## CONDITIONS ON THE BOUNDARY OF THE CORE

The vortex ring propagates with velocity  $-W\hat{\mathbf{k}}$  ( $W \geq 0$ ) and the boundary of its core is impermeable. On the *exterior* side of that boundary the impermeability condition amounts to a Flux/Source condition for  $\Phi$ ; On the *interior* side of that boundary the impermeability condition amounts to a DIRICLET condition for  $\Psi$ .

## CIRCULATION, $C$ , ABOUT THE CORE AND ITS RELATION TO $A$

Consider an oriented close contour  $\mathcal{L}$  that embraces the core once and let  $u_t$  be the tangential component of the fluid velocity on  $\mathcal{L}$ . Define  $C$ —called *the circulation about  $\mathcal{L}$* —by the integral  $\int_{\mathcal{L}} u_t ds$ , in which  $ds$  is the differential arc length on  $\mathcal{L}$  and let  $\delta$  be the radius of a circular disk whose area equals that of a typical cross section of the vortex core. One may then show that

$$A = C / (a\pi\delta^2) .$$

## ON THE FAR FIELD DIPOLE STRENGTH, $G$

Let the fluid velocity,  $\nabla\Phi$ , satisfy  $\nabla\Phi \rightarrow \mathbf{0}$  as  $R \rightarrow \infty$ . If, as here, there are no sources the far field behavior of  $\Phi$  has the asymptotic form

$$\Phi = \Phi_\infty + \mathbf{G} \cdot \nabla[1/(4\pi R)] + O(R^{-3}) ,$$

in which  $\mathbf{G} = \mathbf{G}_1 + \mathbf{G}_2$ , in which

$$\mathbf{G}_1 := \iint_{\mathcal{S}} \Phi \hat{\mathbf{n}} dA \quad , \quad \mathbf{G}_2 := - \iint_{\mathcal{S}} \mathbf{R}(\mathbf{u} \cdot \hat{\mathbf{n}}) dA .$$

Here  $\mathbf{G} = -G\hat{\mathbf{k}}$ ,  $G > 0$ .

## NORMALIZATIONS

Let  $a$  be the value of  $r$  at the centroid of a typical cross section of the ring. In the simulations reported herein I took  $a = 1$  m,  $G = 1$  m<sup>4</sup>/s, and  $\delta = a/2$ .

Let  $\mathbf{v}$  denote the fluid velocity as seen by an observer moving with the ring and let  $\Delta v_t$  be the corresponding slip velocity across the core boundary. In the problem posed herein  $\Phi$ ,  $W$ , and  $C$  are all bilinear functions of the plunge velocity,  $W$  and the circulation  $C$ .

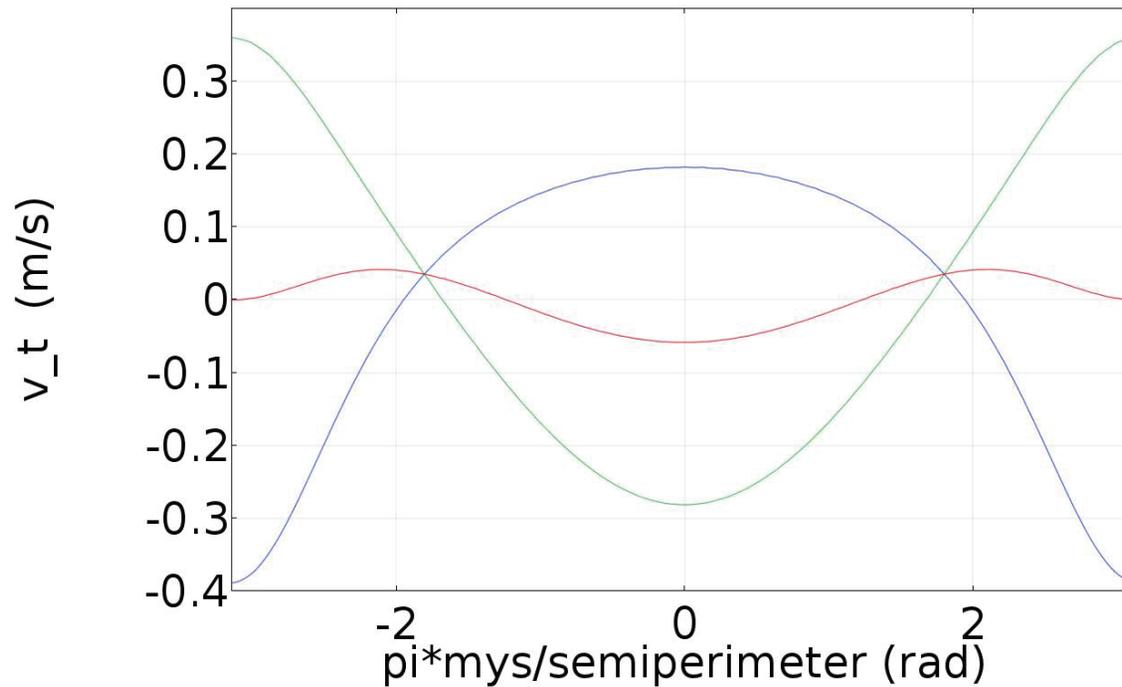
## $(C \quad W)^T$ AS THE SOLUTION OF A MATRIX EQUATION

From the foregoing bilinearity properties we have

$$G_C C + G_W W = G ,$$
$$(\Delta v_t)_C C + (\Delta v_t)_W W = \Delta v_t .$$

If the slip velocity at the inner equator,  $(\Delta v_t)_{ie}$ , is set equal to zero and  $G = 1 \text{ m}^4/\text{s}$  we have

$$\begin{bmatrix} G_C & G_W \\ (\Delta v_t)_{C_{ie}} & (\Delta v_t)_{W_{ie}} \end{bmatrix} \begin{pmatrix} C \\ W \end{pmatrix} = \begin{pmatrix} 1 \text{ m}^4/\text{s} \\ 0 \end{pmatrix} .$$



**Figure 2** Distributions of the slip velocity across the core boundary in three cases, namely: circulation without plunge (green curve), plunge without circulation (blue curve), and circulation and plunge with zero slip at inner equator (red curve)

## USE OF THE MOVING MESH INTERFACE

In the present simulation COMSOL's Geometry Sequence generates a reference core whose cross section is a circular disk of area  $\pi\delta^2$  and centroidal radius  $a$ . COMSOL's Moving Mesh interface then transforms the reference core to one with a general noncircular cross section using formulas derived to ensure that the cross sectional area and the centroidal radius are again equal to  $\pi\delta^2$  and  $a$ , respectively.

## CONTROL VARIABLES

This general noncircular cross section is a (translated and rescaled version of) the interior of the following parametric curve

$$R_{\partial 1} = a + P_{\partial} \cos \alpha \quad , \quad Z_{\partial 1} = P_{\partial} \sin \alpha \quad ,$$

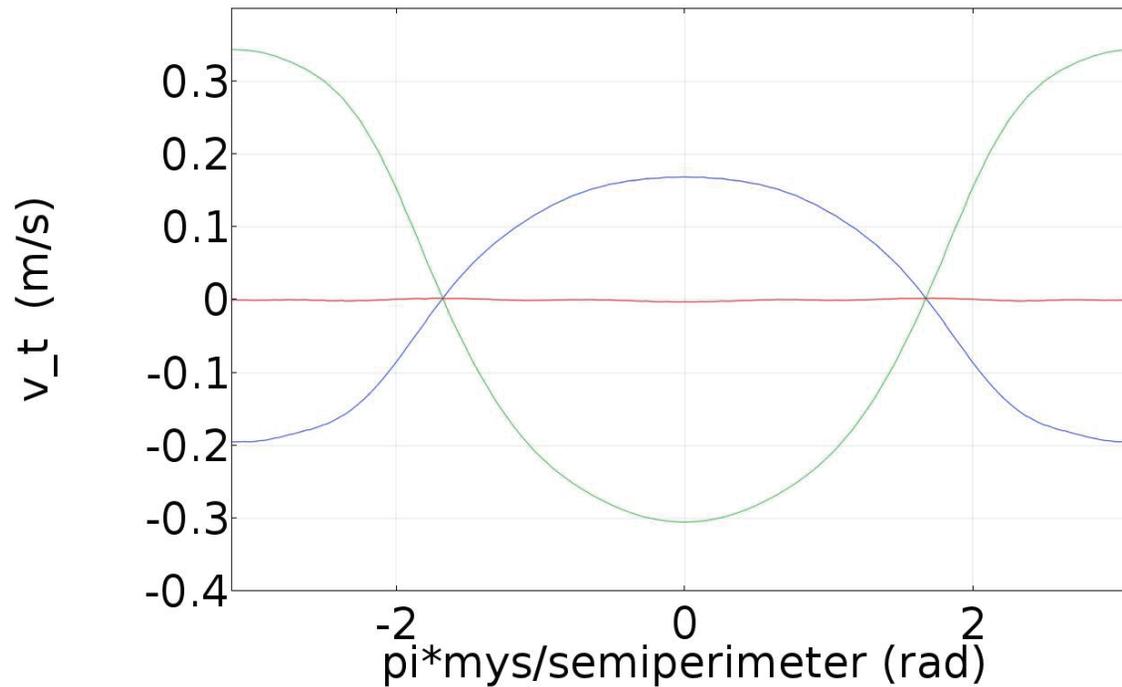
in which  $P_{\partial} = \delta \left[ 1 + \sum_1^N \epsilon_n \cos(n\alpha) \right]$  and in which the coefficients  $\epsilon_n$ ,  $n \in \{1, \dots, N\}$  are shape parameters that will be control variables in an optimization problem.

## OBJECTIVE FUNCTION

The objective function  $F$  in the optimization problem is

$$F = C^{-2} \int_{\partial \mathcal{D}^c} (\Delta v_t)^2 ds \cdot \int_{\partial \mathcal{D}^c} ds$$

in which  $\mathcal{D}^c$  is a typical meridional cross section of  $\mathcal{R}^c$ .



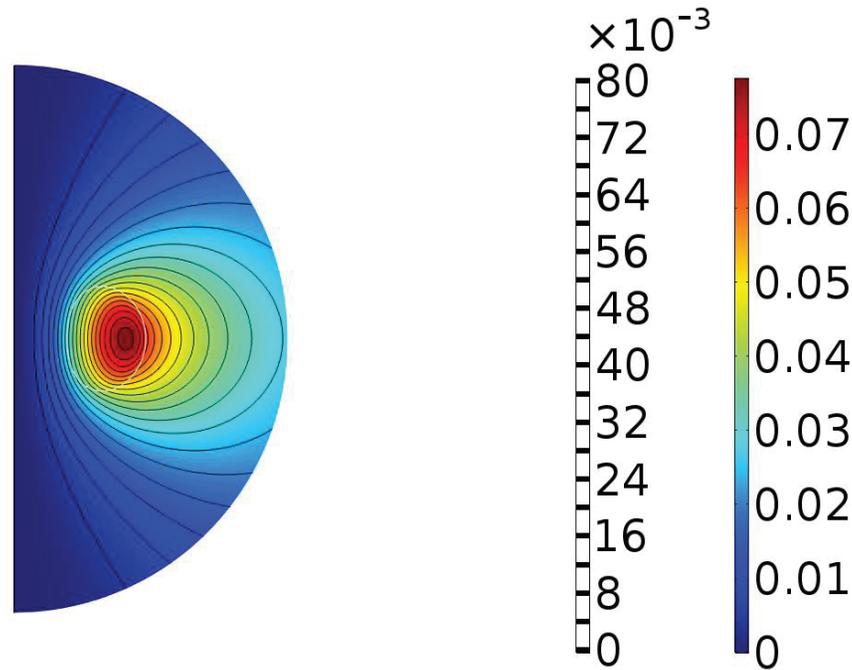
**Figure 3** Legend same as that of Fig. 2 except that this time, the results shown are for a non-circular core shape after optimization to minimize slip across the core boundary in the case of circulation and plunge with zero slip at inner equator.

## COMPUTATION OF $\Psi$ IN $\mathcal{R}^i \setminus \mathcal{R}^c$

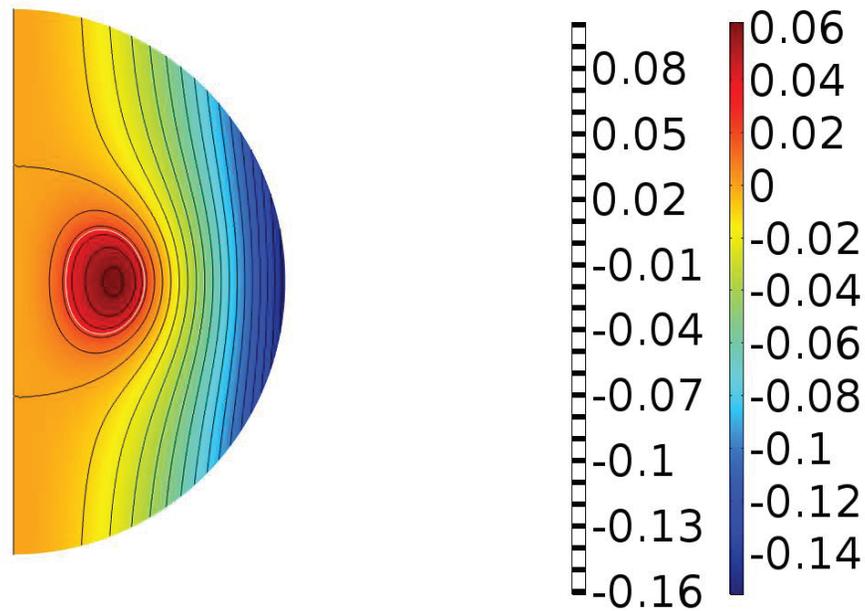
Having  $u_r = \partial\Phi/\partial r$  and  $u_z = \partial\Phi/\partial z$  in  $\mathcal{R}^i \setminus \mathcal{R}^c$   
I computed the corresponding STOKES stream function  $\Psi$  by specifying

$$\left( \frac{\partial\Psi}{\partial r} + ru_z \right) \text{test} \left( \frac{\partial\Psi}{\partial r} \right) + \left( \frac{\partial\Psi}{\partial z} - ru_r \right) \text{test} \left( \frac{\partial\Psi}{\partial z} \right)$$

in the input field for a Weak Form PDE Physics interface. I set  $\Psi = 0$  on  $r = 0$  (all  $z$ ) and accepted the default Null Flux boundary conditions on the core boundary and the portal.



**Figure 4**  $\Psi$  in  $\mathcal{D}^i$  relative as seen by an observer at rest relative to the remote undisturbed fluid. The white contour is the core boundary. The increment of  $\Psi$  between contours is  $0.04 \times 10^{-3} G/a^2$ .



**Figure 5** Legend similar to that of Fig. 4, except that now the results are as seen by an observer propagating with the ring.