

Thermal-Fluid Dynamic FEM Simulation of Advanced Water Cold Plates for Power Electronics



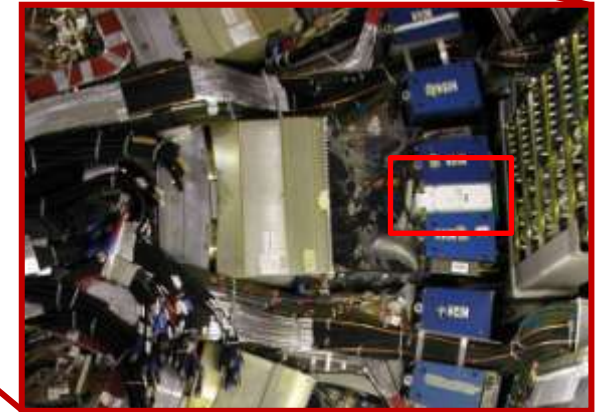
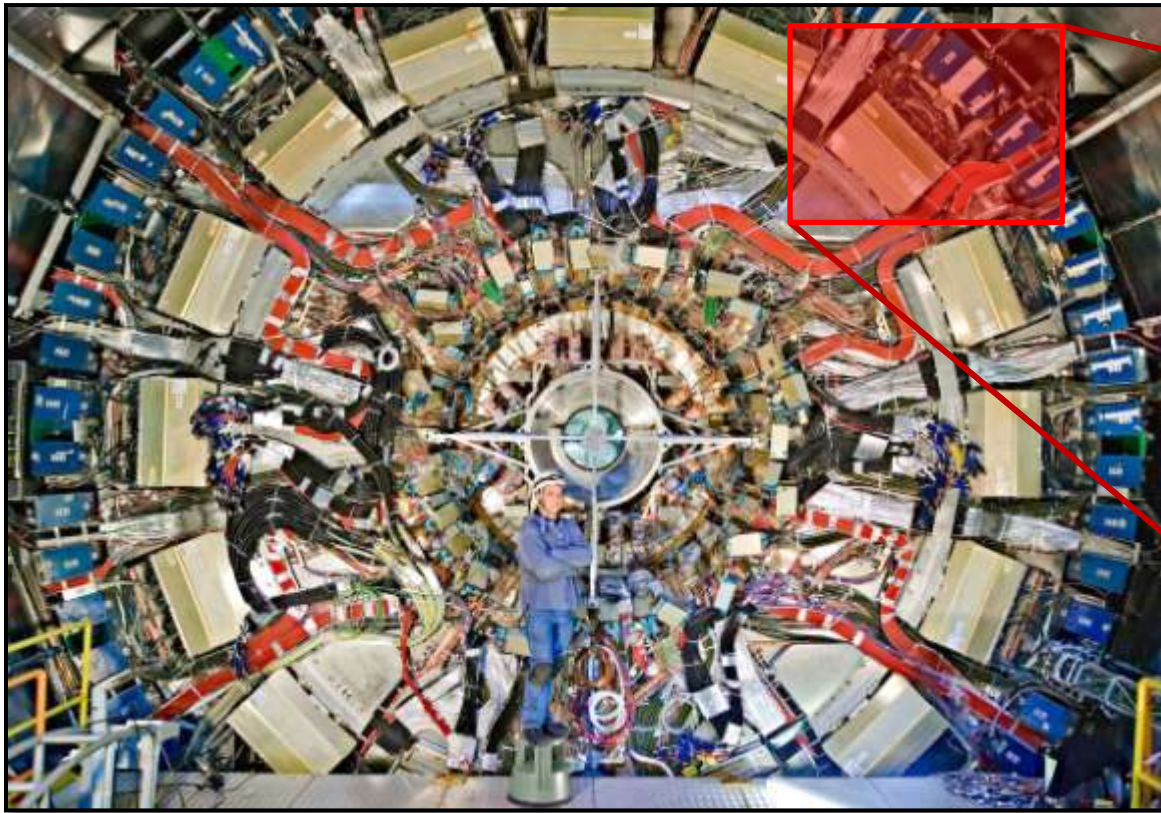
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Purpose of the work

Thermal design of power supplies for application in high energy physics experiments: cold plate optimization



System thermal constraints

DC-DC main converter: 280-12 V, $P_{\text{out}} = 3 \text{ kW}$

3 modules 1.5 kW each

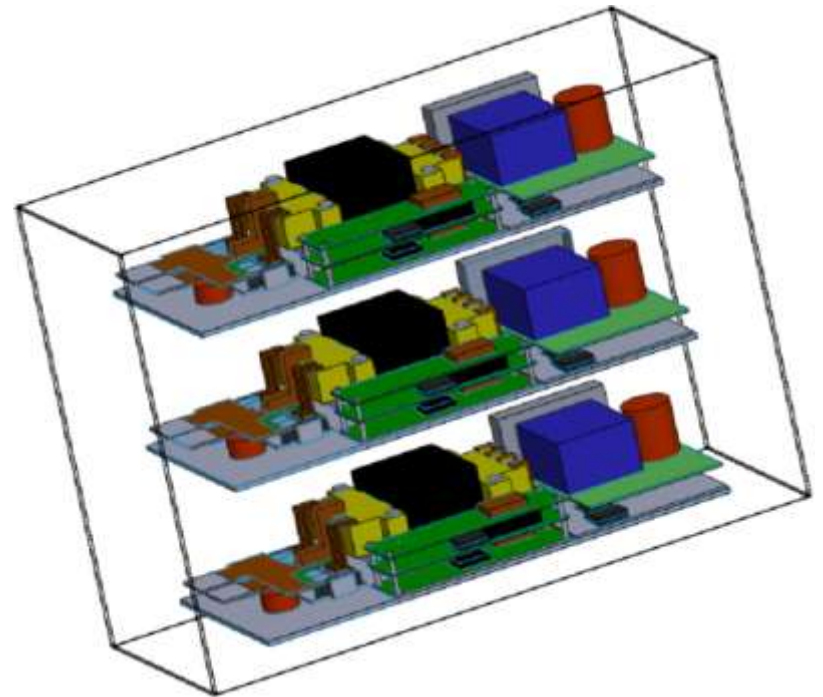
Redundancy 2+1:

- nominal condition: 3 x 1 kW
- one module failed: 2 x 1.5 kW

Worst case efficiency: $\eta = 79\%$

Dissipated power = 800 W

- nominal condition: 3 x 267 W
- one module failed: 2 x 400 W



Each module cooled by its own water heat sink

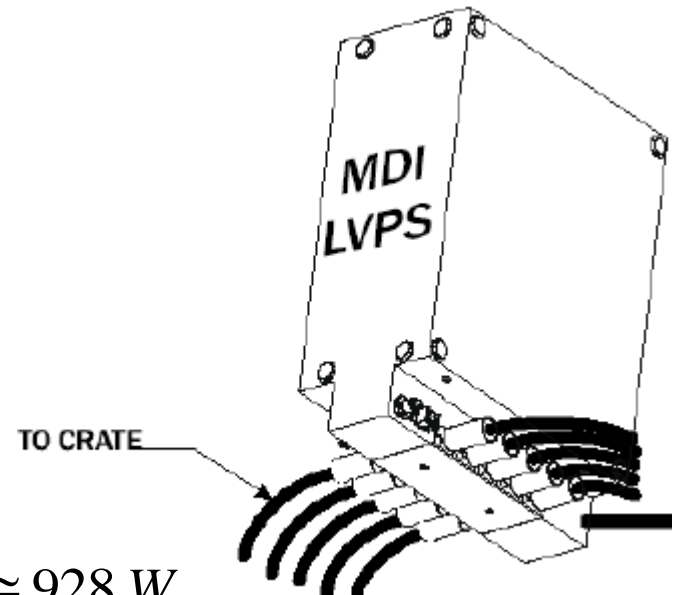
System thermal constraints

DC-DC main converter: 280-12 V, $P_{\text{out}} = 3 \text{ kW}$

- Case: 150 x 402 x 285 mm³, steel 1510
- Water cooling system:
 - *delivery* = 1.9 l/min,
 - $\Delta p \leq 350 \text{ mbar}$
 - $T_{\text{inlet}} = 18 \text{ }^\circ\text{C}$; $T_{\text{outlet}} \leq 25 \text{ }^\circ\text{C}$
- Maximum heat flux:

$$Q_{H_2O \text{ flow}} = C_p \cdot \Delta T \cdot \textit{delivery} = 4186 \cdot 7 \cdot \frac{1.9}{60} \cong 928 \text{ W}$$

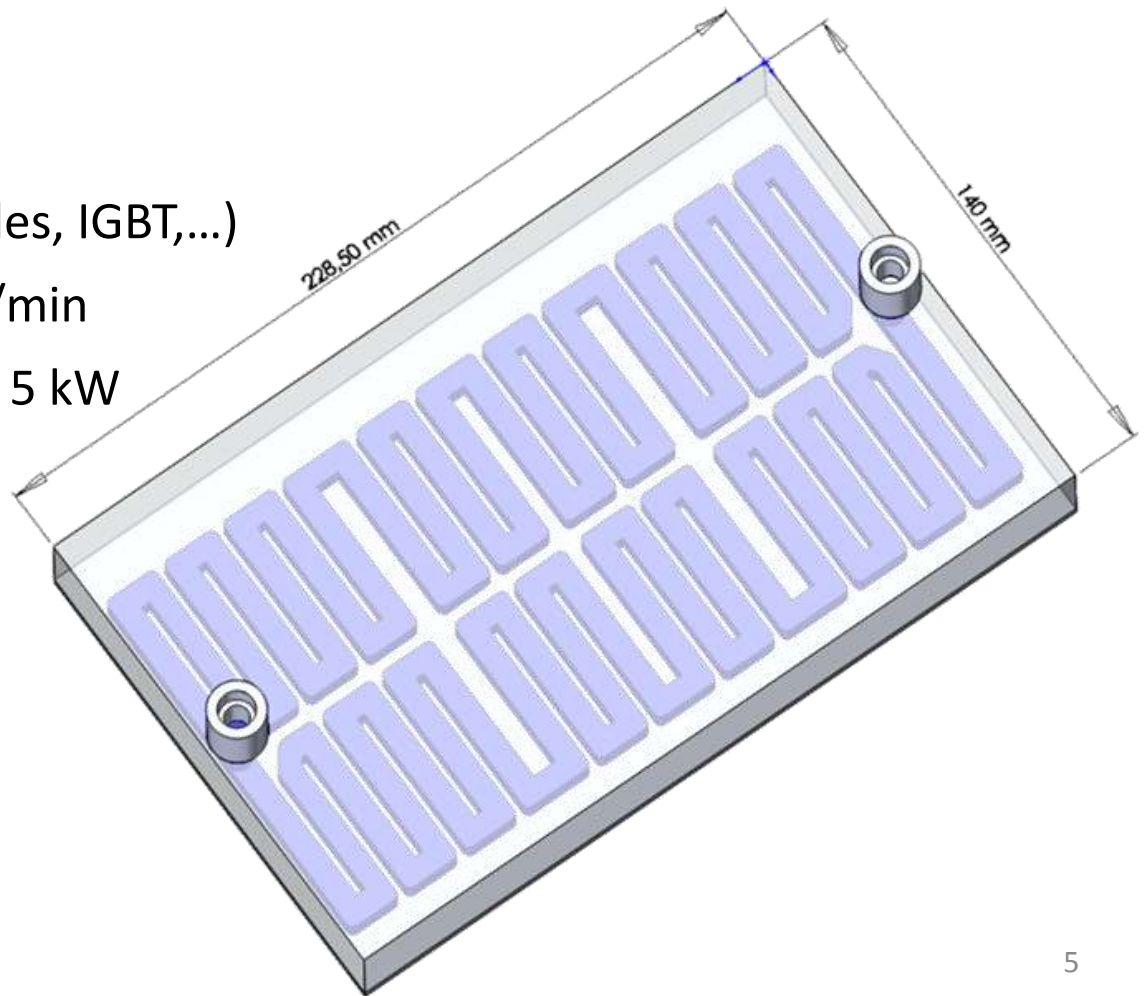
- Room temperature = 18 °C
- Maximum case external temperature: 20 °C, stable



Modeling validation

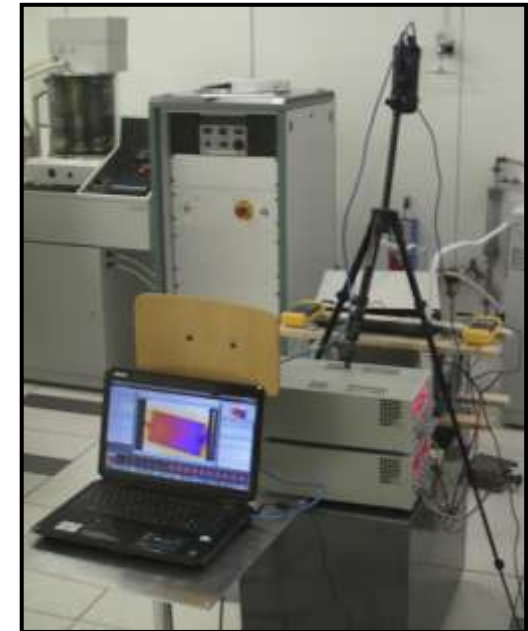
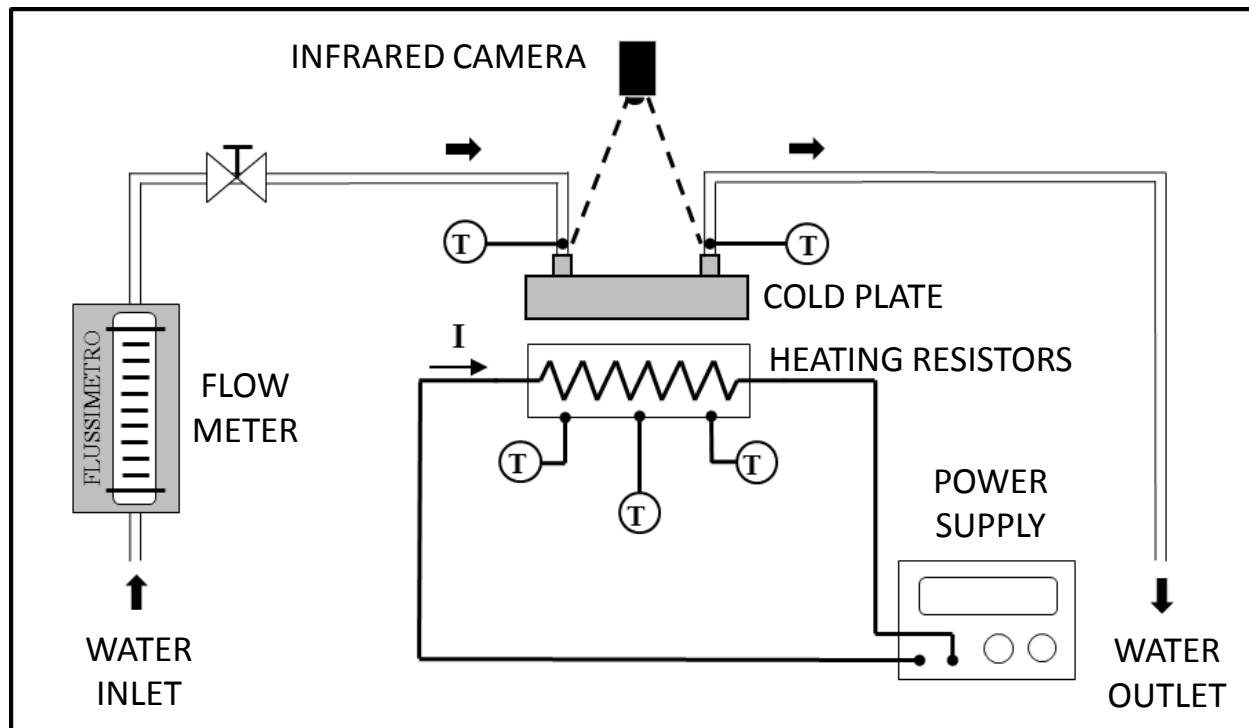
POSEICO AWCH_L228W140T28

- Aluminum cold plate
- Coolant: water
- Power devices (PiN diodes, IGBT,...)
- Maximum flow rate: 9 l/min
- Dissipated power: up to 5 kW



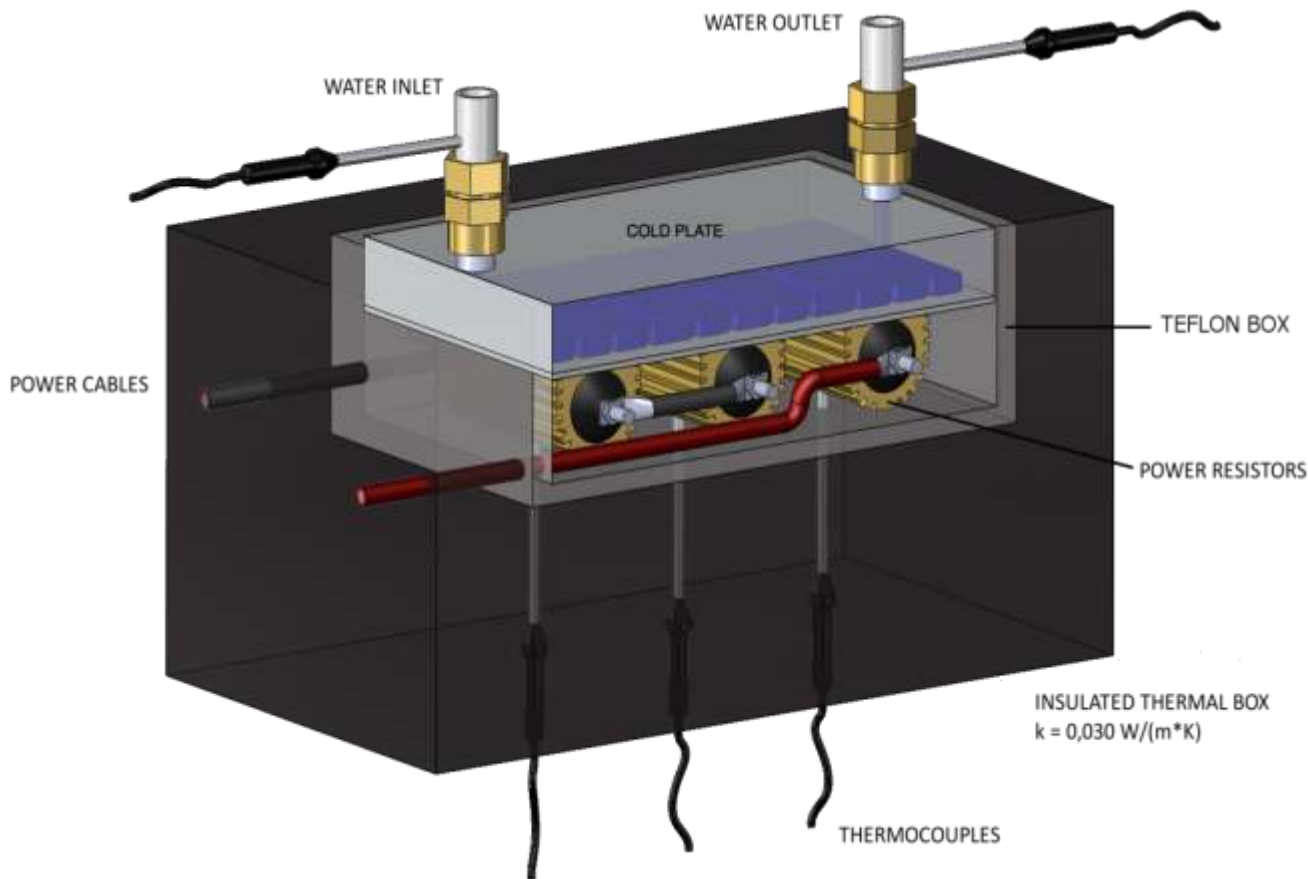
Modeling validation

Experimental characterization: test bench



Modeling validation

Experimental characterization: heating set up



Heat sources

- 3 Power resistors
- $R = 0.1 \Omega$ (200 W)
- $P_{\max} = 600 \text{ W}$

Insulation

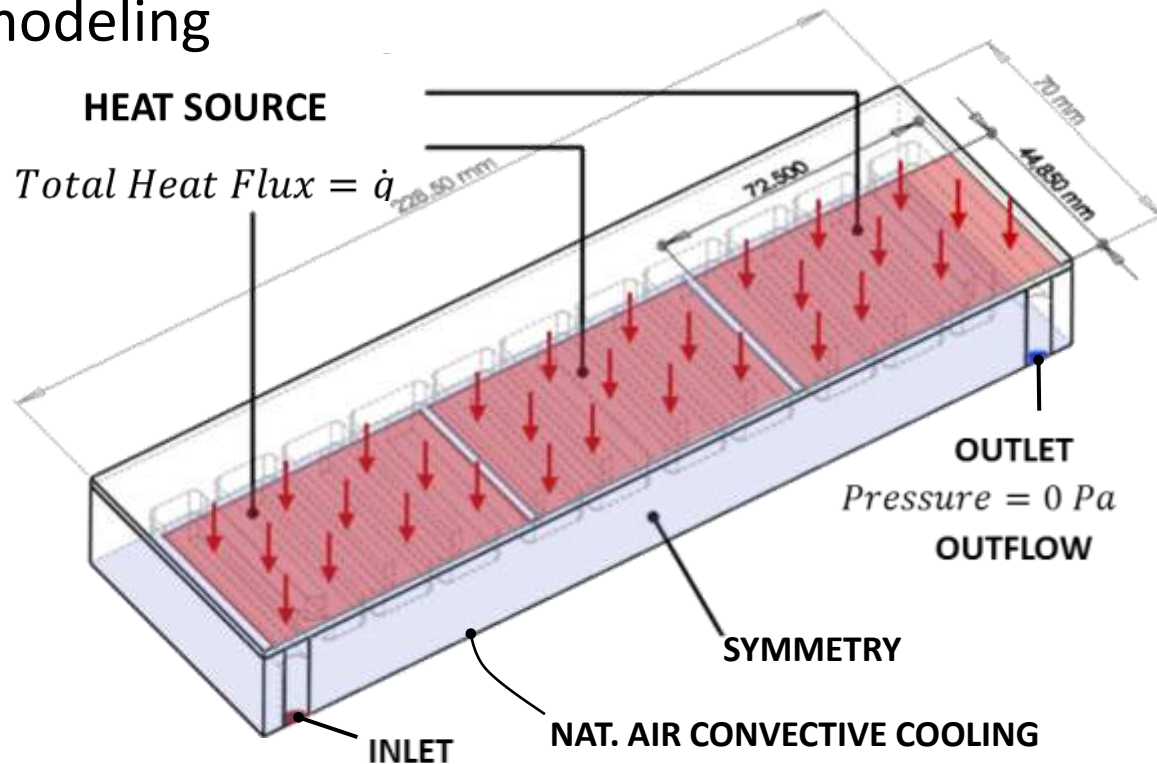
- Teflon-Polystyrene insulator box
- $P_{\text{loss}} < 2 \text{ W}$

Modeling validation

Numerical analysis: FE modeling

HT+CFD fully coupled model

$Re < 4300$  Laminar Flow



Boundary conditions

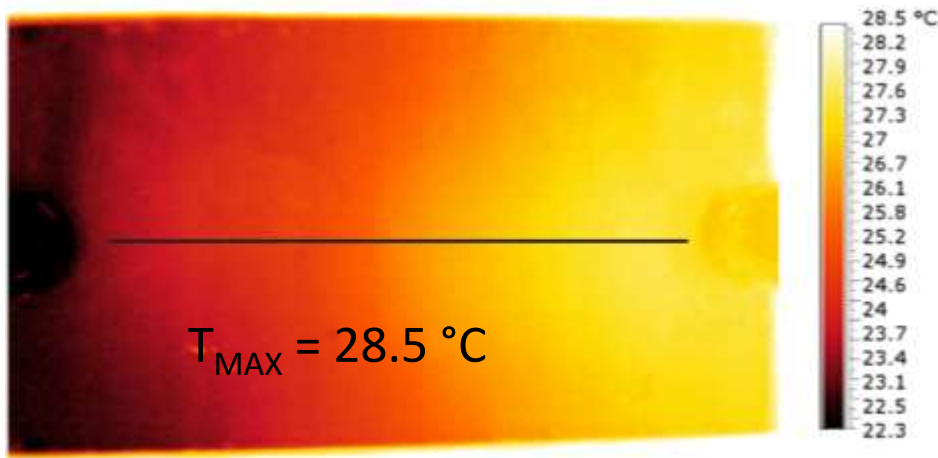
Mean Inlet Velocity	v_{inlet}	0.436 m/s
Inlet Temperature	T_{inlet}	18.8 °C
Total Heat Flux	T_{inlet}	28600 W/m ²
External Temperature	T_{amb}	31 °C

$$v = v_{inlet} ; T = T_{inlet}$$

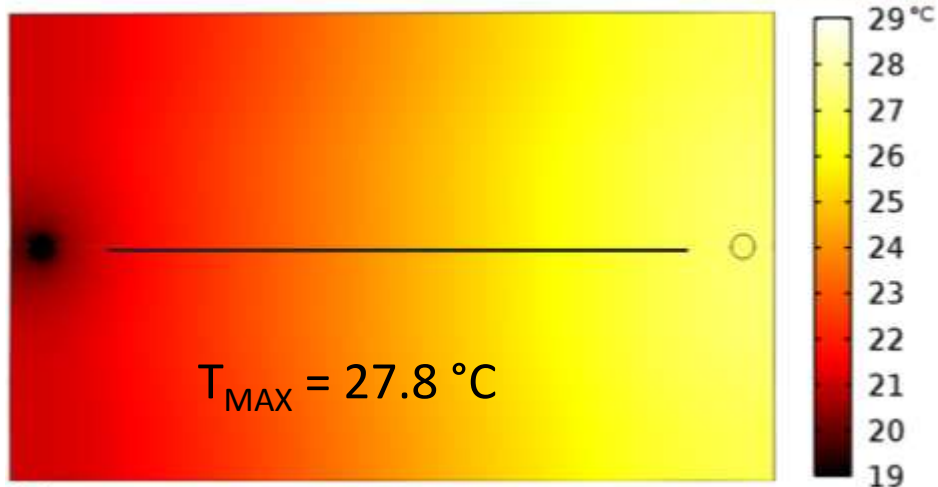
 **558 W**

Modeling validation

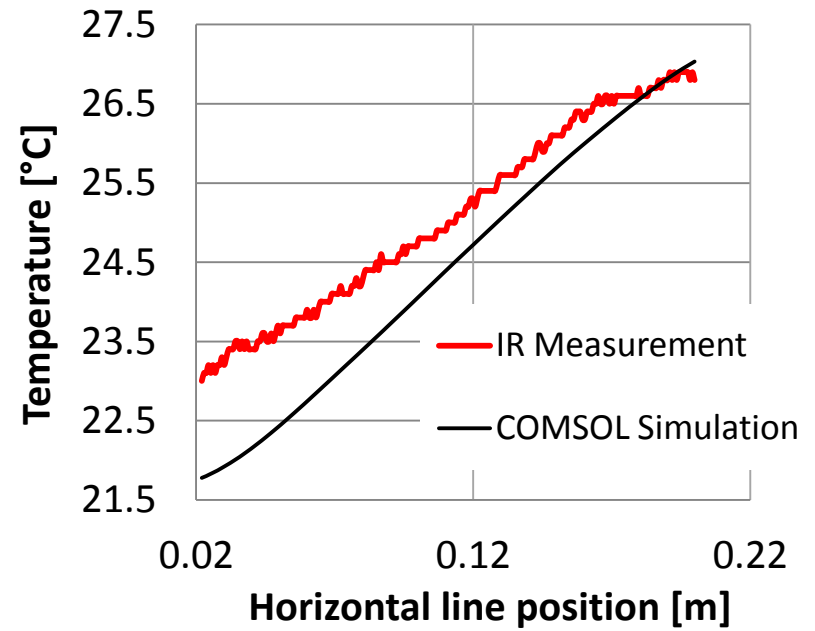
Simulations vs. Measurements



(a)

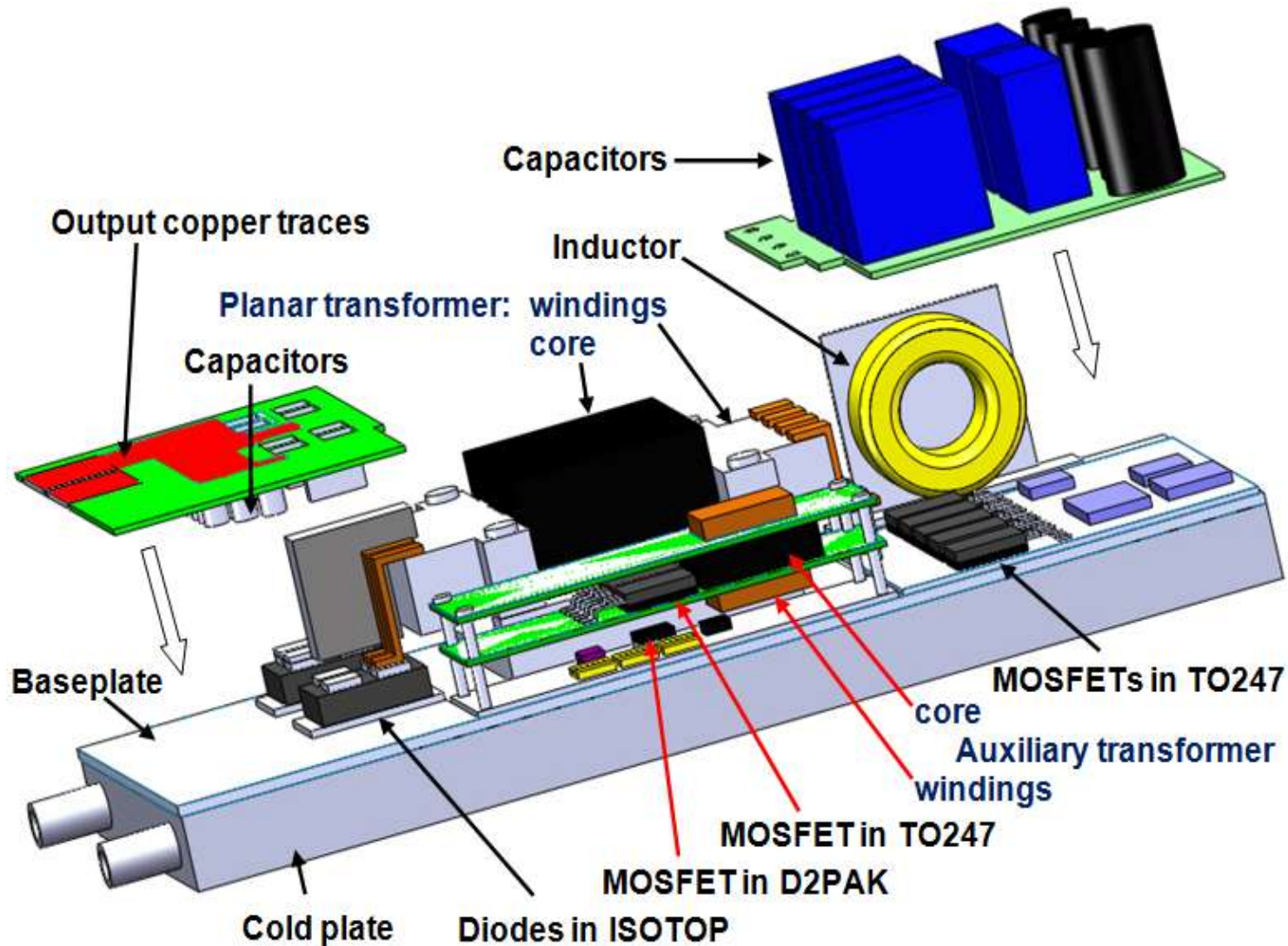


(b)



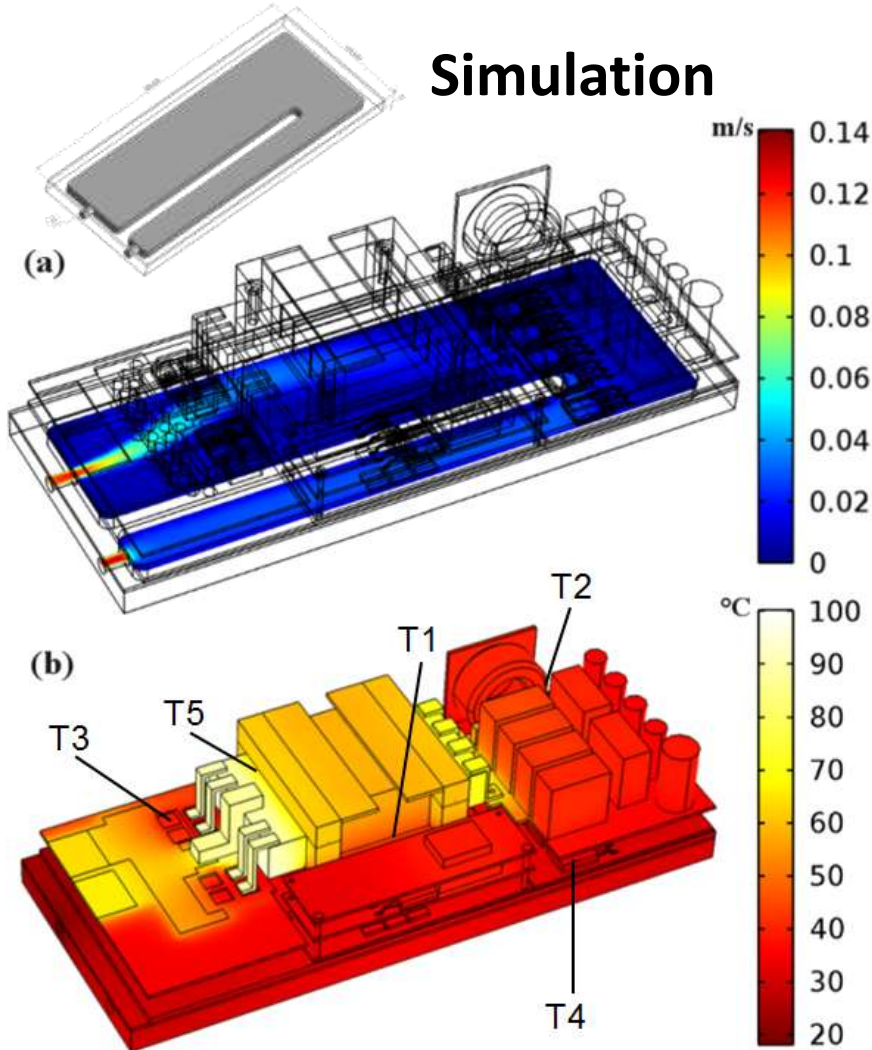
	T_{inlet}	T_{outlet}	ΔT
Thermocouple	18.8 °C	24.8 °C	6.0 °C
COMSOL	18.8 °C	25.6 °C	6.8 °C

Power module thermal modeling



Power module thermal modeling

Simulation

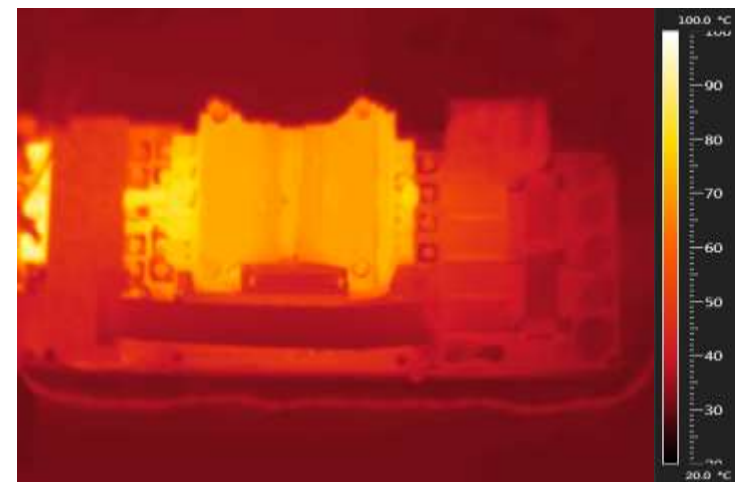


$P_{out} = 1.2 \text{ kW}$

$P_d = 240 \text{ W}$

	Thermocouple	COMSOL
T1	35.1 °C	37.8 °C
T2	36.7 °C	37.3 °C
T3	37.5 °C	38.4 °C
T4	40.0 °C	39.1 °C
T5	77.2 °C	75.7 °C

IR measurement

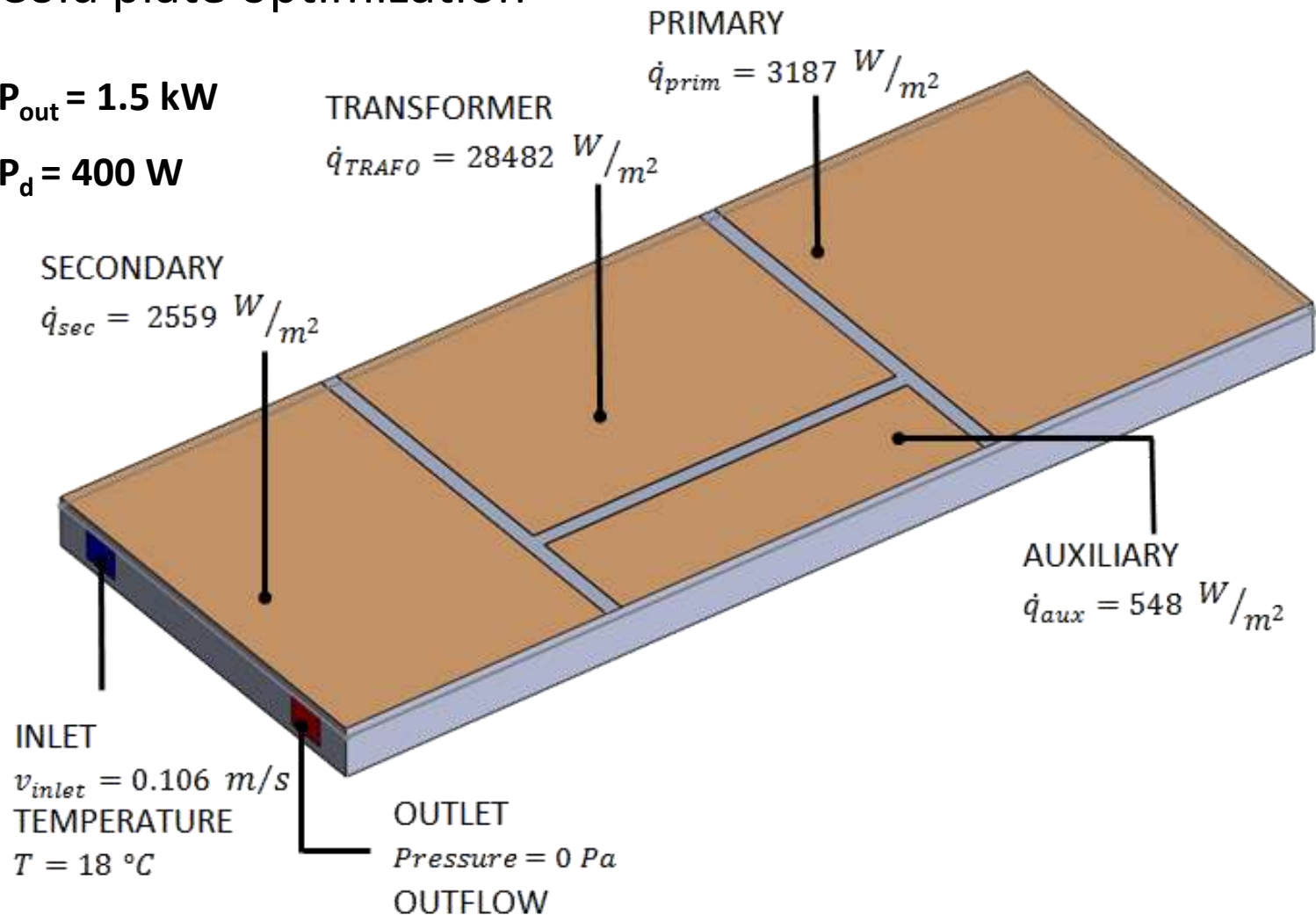


Power module thermal modeling

Cold plate optimization

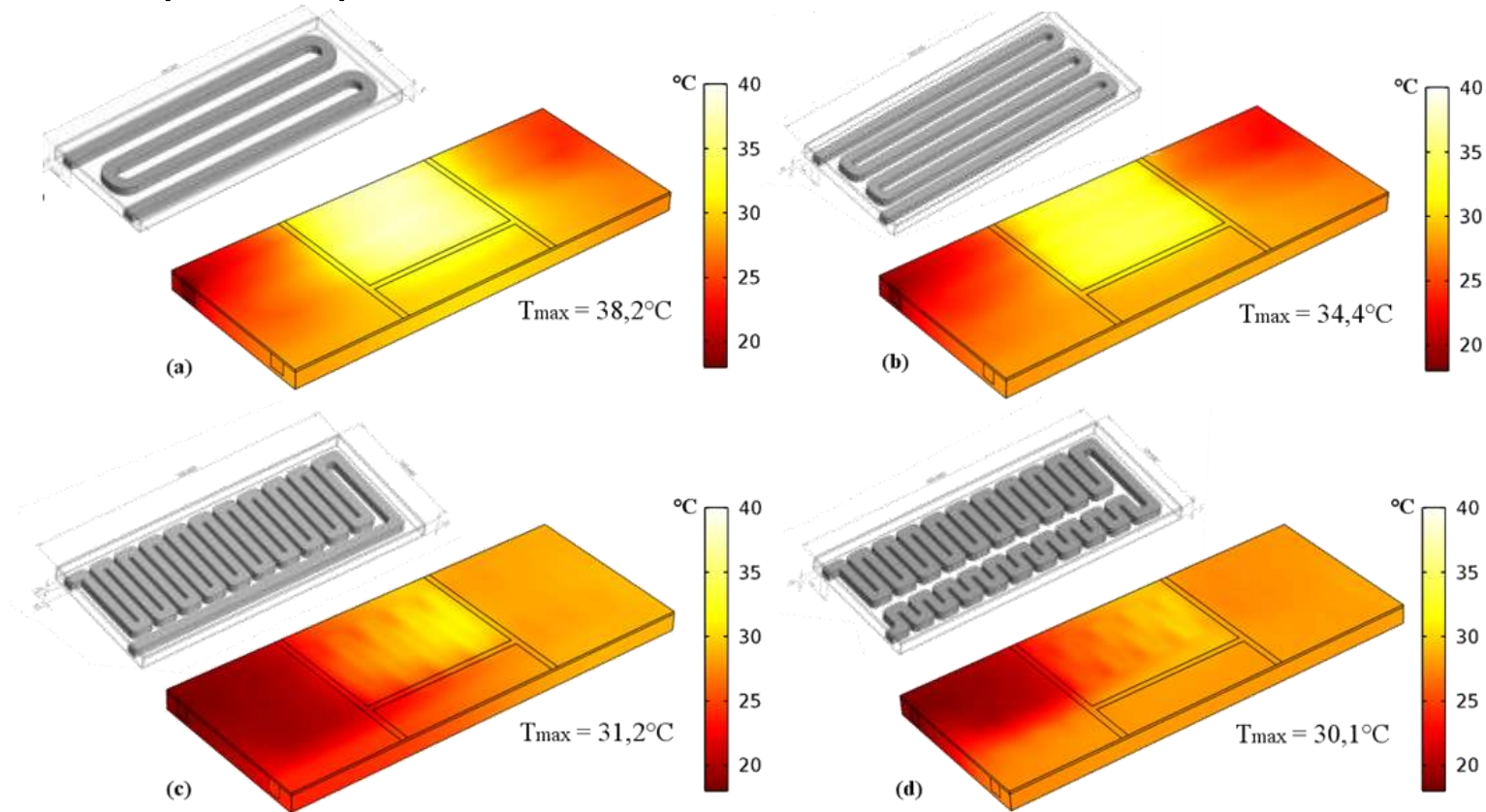
$P_{out} = 1.5 \text{ kW}$

$P_d = 400 \text{ W}$



Power module thermal modeling

Cold plate optimization



$P_{\text{out}} = 1.5 \text{ kW}$

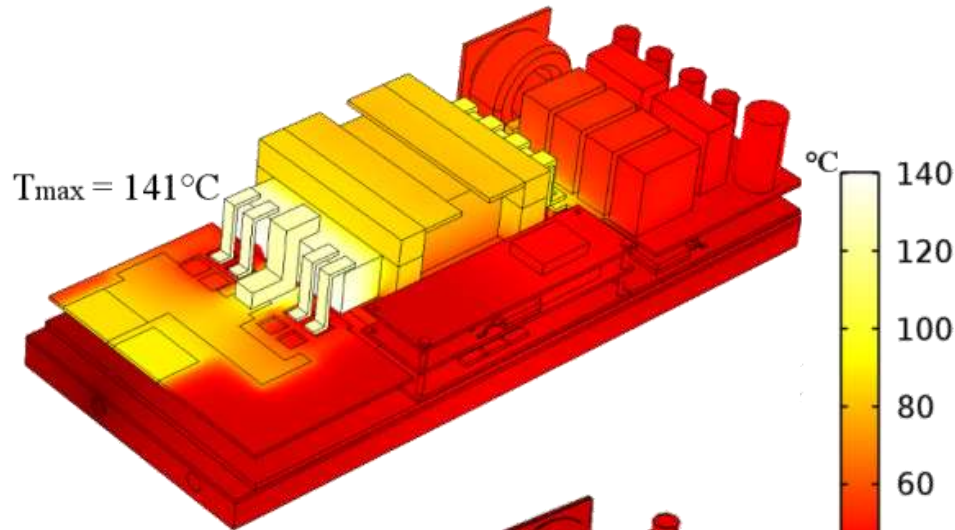
$P_{\text{d}} = 400 \text{ W}$

Pattern	(a)	(b)	(c)	(d)
T_{outlet}	24.8 °C	27.4 °C	26.8 °C	27.2 °C

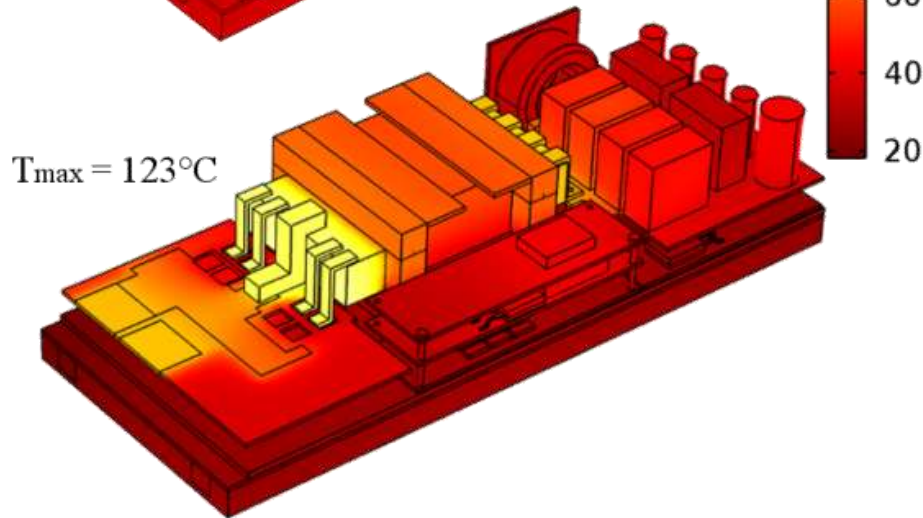
Power module thermal modeling

$P_{out} = 1.5 \text{ kW}$

$P_d = 400 \text{ W}$



“U shaped” cold plate



New cold plate type (a)

Conclusions

- FE simulations of a complex power converter with coupled HT-CFD solution has been shown.
- The approximations introduced to simplify the models without losing accuracy were validated with ad-hoc test bench and measurements.
- Searching for the optimum cold plate, has been found that for the current converter the power to dissipate is too much high.
- Improvement of the converter efficiency and further optimization of the cold plate are needed.

Thank you