

Modeling of Non-isothermal Reacting Flow in Fluidized Bed Reactors

V. Orava¹, O. Souček², P. Cendula¹

¹Institute of Computational Physics, ZHAW, Winterthur, Switzerland

²Faculty of Mathematics and Physics, Charles University in Prague, Prague, Czech Republic

Abstract

Abstract:

We investigate a prototype concept of a back-up electricity device where we use liquid formic acid (FA) to produce a mixture of carbon dioxide (CO₂) and hydrogen (H₂) which is used in a PEM fuel cell, Fig. 1. In the fluidized bed reactor the liquid FA is decomposed to a gaseous mixture of CO₂ and H₂ in the presence of microscopic floating solid catalytic particles. We describe the system, contained in a fixed control volume, as a mixture composed of five constituents - liquid FA, gaseous FA (FAG), catalyst micro-particles (Cat), CO₂ and H₂. For the individual mixture components, we distinguish partial densities and momenta, while we only consider one common temperature field for the mixture as a whole. We reduce the five-constituents model to a binary mixture model of liquid phase (Cat + FA) and gaseous phase (CO₂ + H₂ + FAG) which forms bubbles. The liquid phase is considered as a compressible viscous fluid with temperature-dependent density and viscosity depending on both the temperature (Arrhenius model) and the volume fraction of the catalyst particles. The gaseous phase is considered as an ideal gas mixture where the molar-ratio of H₂ and CO₂ is 1:1. Since we assume local gas/liquid equilibrium where the liquid is already saturated by all three gaseous constituents, the amount of FAG in the bubbles depends on the saturation pressure (i.e. temperature and ambient pressure) and any interfacial mass flow is neglected. Chemical rates satisfy mass-action law and follow the Arrhenius kinetics. The quasi-steady model was implemented numerically in COMSOL Multiphysics and we present several simulations addressing primarily the role of saturation pressure and another important dependencies.

Keywords: multi-phase flow, fluidized bed reactor, gas-liquid equilibrium, bubbly flow, bubble growth

Use of COMSOL Multiphysics®:

We implemented the model using combination of "Laminar Bubble Flow" and "Heat Transfer in Fluids" Physics both included in CFD module. We defined material properties of the two phases, i.e. gaseous mixture (FA, H₂, CO₂) and mixture of liquid FA with catalytic particles. Their material properties were defined in way to realistically describe various dependencies. Furthermore, we redefine the bubble flow model according to Karamanev and we introduced some implicit constitutive relations. Here we have to introduce additional step in segregated solver by adding auxiliary PDE's - this can be also understand as additional stabilization.

Reference

- [1] V. Orava, O. Soucek, P. Cendula, Multi-phase modeling of non-isothermal reactive flow in fluidized bed reactors, *Journal of Computational and Applied Mathematics*, 2015.
- [2] H.A. Jakobsen, *Chemical Reactor Modeling: Multiphase Reactive Flows*, Springer, 2008.
- [3] W.C. Yang, *Handbook of Fluidization and Fluid-Particle Systems*, Taylor & Francis, 2003.
- [4] W. M. Haynes, *CRC Handbook of Chemistry and Physics*, CRC Press, 2014.
- [5] D.G. Karamanev, Equations for calculation of the terminal velocity and drag coefficient of solid spheres and gas bubbles, *Chem. Eng. Comm.*, 1996.
- [6] C. Antoine, Vapor Pressure: a new relationship between pressure and temperature, *Comptes Rendus des Séances de l'Académie des Sciences* (in French), 1888.
- [7] M.S. Silberberg, *Chemistry : the molecular nature of matter and change* (5th ed. ed.), Boston: McGraw-Hill, 2009.
- [8] R. Sander, Compilation of Henry's law constants, *Atmos. Chem. Phys. Discuss.*, 2014

Figures used in the abstract

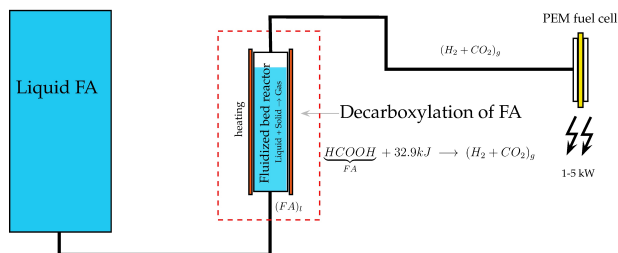


Figure 1: Schema of the device.

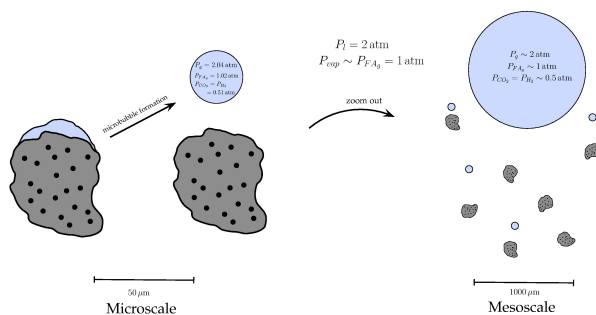


Figure 2: Bubble formation.