## **Several Hydrodynamic Instabilities** OMSOLIllustrated Using COMSOL Multiphysics® Cornelius F. Ivory 2018 Boston Voiland School of Chemical Engineering and Bioengineering Washington State University, Pullman WA, 99163



**INTRODUCTION:** COMSOL Multiphysics<sup>®</sup> has proved invaluable for teaching "Transport Phenomena" to graduate and undergraduate engineers. This software allows us to visualize and explore solutions well beyond what could be done with pencil and paper. One of the topics that had previously been skipped, due to the complexity of the mathematics, was hydrodynamic instabilities. Using COMSOL, students are able to locate the point of neutral stability and then visualize changes in the system as the instability emerges, amplifies itself and then progresses to a secondary state.

**RESULTS**: Fig. 2 shows the secondary (left) and tertiary (right) flows that develop in a Couette viscometer when the dimensionless rotation rate, as characterized by the Taylor number, exceeds a a first (left) and then a second (right) critical value.





**Figure 1**. *Left*: Buoyancy-induced instability<sup>1</sup> in a thin film of water with the no-slip condition applied on all container surfaces and with surfaces heated from below, cooled from above and insulated on the sides. This system was modeled using equations [1-3].

*Right*: Nusselt number vs Rayleigh number plot showing the emergence of a secondary heat transfer mechanism near Ra=2500. **Figure 2**. *Left*: Centrifugual instability<sup>3</sup> showing steady Taylor vortices formed in the annulus between a rotating inner cylinder and a fixed outer cylinder when the rotation rate exceeds a critical RPM. *Right*: An oscillatory instability appears after a second critical Taylor number is reached. The flow is still laminar here so simulation is possible. This system was modeled using equations [1-2].





**COMPUTATIONAL METHODS**: All of the secondary flows shown in this poster were generated using some combination of the following equations as indicated in each figure caption. [1] the Navier-Stokes equation, [2] the Continuity equation, [3] the Thermal Energy equation and [4] the charge conservation equation.<sup>2</sup>

$$\rho \frac{\partial \boldsymbol{u}}{\partial t} + \rho \boldsymbol{u} \cdot \nabla \boldsymbol{u} = -\nabla p + \nabla \cdot \boldsymbol{\mu} \nabla \boldsymbol{u} + \rho \boldsymbol{g}$$
[1]

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho u = \mathbf{0}$$
 [2]

$$\rho C_{p} \frac{\partial T}{\partial t} + \rho C_{p} \boldsymbol{u} \cdot \nabla T = \nabla \cdot k \nabla T + \sigma \boldsymbol{E} \cdot \boldsymbol{E}$$
[3]

$$\frac{\partial q}{\partial t} + \nabla \cdot \sigma \boldsymbol{E} = \boldsymbol{0}$$
[4]

Figure 3. Left: Buoyancy instability showing roll vortices in a Clusius-Dickel column<sup>2</sup> heated on the right and cooled on the left. This system was modeled using equations [1-3]. *Right*: Oscillatory instability in a continuous flow electrophoresis device with Joule heating. This system was modeled using equations [1-4].

**CONCLUSIONS**: Transport instabilities that can be modeled using the equations of conservation can be readily simulated using COMSOL Multiphysics v5 so long as the secondary state is laminar. Generally, these simulations take less than an hour to set up; they run to completion in 10s of minutes for 2D problems or several hours for 3D problems, depending on their complexity.

These bulk equations were solved together with the "no-slip" condition and with prescribed heat fluxes applied on all solid boundaries. The charge conservation equation assumed constant electrical conductivity, fixed potentials on the anode and cathode with all other surfaces electrically insulating. In all cases the initial conditions specified zero velocity and uniform temperatures throughout the computational domain.

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