

Analysis of Lubricant Flow through Reynolds Equation

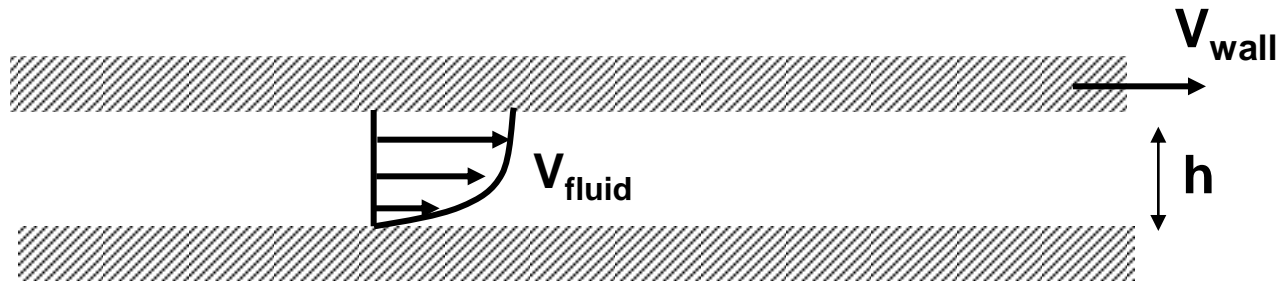
J.S. Crompton, L.T. Gritter, S.Y. Yushanov, K.C. Koppenhoefer
AltaSim Technologies, LLC

R.O. Edwards
Cummins Fuel Systems, Inc.

COMSOL Conference – October, 2010



What is Reynolds Equation?



- Special case of Navier-Stokes Equations
 - 1) fluid thickness small compared to length/width,
 - 2) pressure gradients through fluid thickness are small,
 - 3) no external forces act on the fluid film,
 - 4) no slip at the bearing surfaces, and
 - 5) velocity gradients along the thickness dominate all other velocity gradients.

Applications

- Common solution to tribology problems
- Thin layer of fluid reduces friction/wear



Why COMSOL?

- Designed for multiphysics problems
- Designed for simple implementation of “new” physics
 - PDE mode
 - Weak boundary conditions
 - Boundary extrusion coupling variables (calculate h)

Procedure

- Implement Reynolds Equation in COMSOL Multiphysics
- Include thermodynamics of fluid properties
- Verify w/ existing solution for simple case

Reynolds Equation – Weak Form

Reynolds equation:
$$\frac{\partial}{\partial x} \left(\frac{\rho h^3}{\eta} \frac{\partial P}{\partial x} \right) + \frac{\partial}{\partial y} \left(\frac{\rho h^3}{\eta} \frac{\partial P}{\partial y} \right) = 6 \frac{\partial}{\partial x} (\rho U_0 h) + 6 \frac{\partial}{\partial y} (\rho V_0 h) + 12 \rho W_0$$

or
$$\frac{\partial}{\partial x} \left(\frac{\rho h^3}{12\eta} \frac{\partial P}{\partial x} - \frac{1}{2} \rho U_0 h \right) + \frac{\partial}{\partial y} \left(\frac{\rho h^3}{12\eta} \frac{\partial P}{\partial y} - \rho V_0 h \right) = \rho W_0$$

where

h gap

U_0, V_0, W_0 velocity components of gap boundary

Equivalent form or Reynolds equation:
$$\nabla \cdot (-\mathbf{q}) = \rho W_0$$

$$\mathbf{q} = \left\{ \rho \left(\frac{U_0 h}{2} - \frac{h^3}{12\eta} \frac{\partial P}{\partial x} \right), \rho \left(\frac{V_0 h}{2} - \frac{h^3}{12\eta} \frac{\partial P}{\partial y} \right) \right\}$$
 mass flow rate per unit width $\left[\frac{\text{kg}}{\text{m} \cdot \text{s}} \right]$

Reynolds Equation – Weak Form

Multiply Reynolds equation by test/shape function P_{test} and integrate over domain Ω :

$$\int_{\Omega} P_{test} \nabla \cdot (-\mathbf{q}) d\Omega = \int_{\Omega} P_{test} \rho W_0 d\Omega$$

• use identity $\nabla \cdot (P_{test} \mathbf{q}) = P_{test} \nabla \cdot \mathbf{q} + \mathbf{q} \cdot \nabla P_{test}$
 • use Gauss theorem: $\int_{\Omega} \nabla \cdot (P_{test} \mathbf{q}) d\Omega = \int_{\partial\Omega} P_{test} \mathbf{q} \cdot d\mathbf{n}$

$$\left. \begin{array}{l} \int_{\partial\Omega} P_{test} \mathbf{q} \cdot d\mathbf{n} - \int_{\Omega} \mathbf{q} \cdot \nabla P_{test} d\Omega = \int_{\Omega} P_{test} \rho W_0 d\Omega \end{array} \right\} \rightarrow$$

\mathbf{n} : unit normal to boundary

• introduce Lagrange multiplier μ

• assume Neumann BC: $-\mathbf{n} \cdot \mathbf{q}|_{\partial\Omega} = G + \mu H$

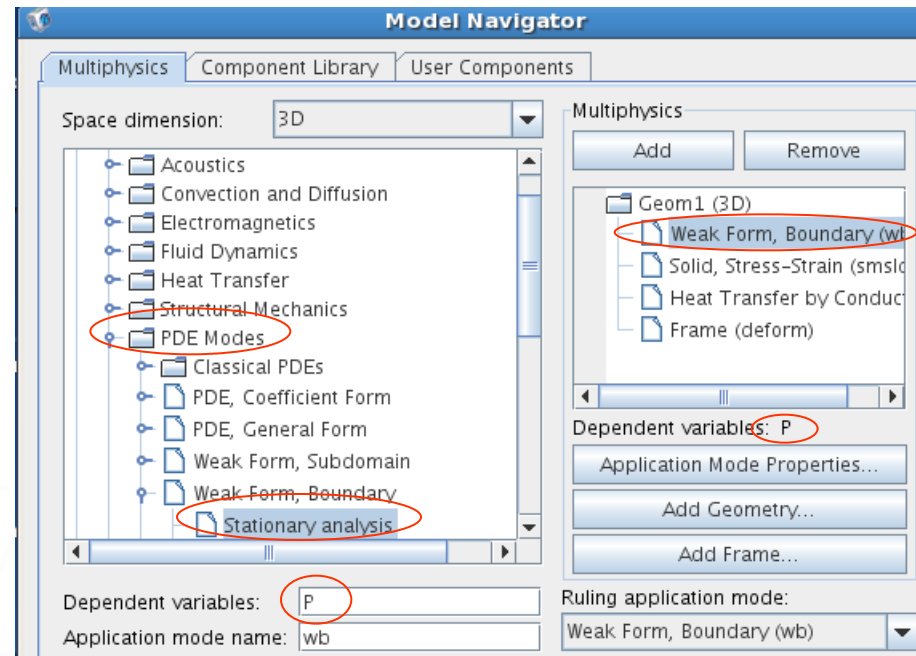
Complete weak form formulation of Reynolds equation:

$$\begin{cases} 0 = \int_{\Omega} (\nabla P_{test} \cdot \mathbf{q} + P_{test} \rho W_0) d\Omega + \int_{\partial\Omega} P_{test} (G + \mu H) dn \\ 0 = (P_0 - P)|_{\partial\Omega_1} \quad \text{Dirichlet BC} \end{cases}$$

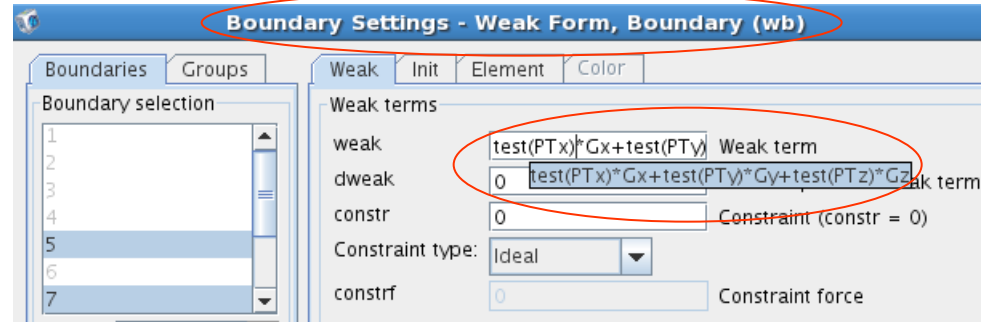
Reynolds Equation – COMSOL

v3.5a

- Weak Form Boundary Mode :



Reynolds Equation - COMSOL



•Type in Reynolds equation in weak form for gap boundaries:

$$\frac{\partial P}{\partial x} = PTx$$

$$\frac{\partial P_{test}}{\partial x} = test(PTx)$$

G_x, G_y is mass flow rate (defined as global variables)

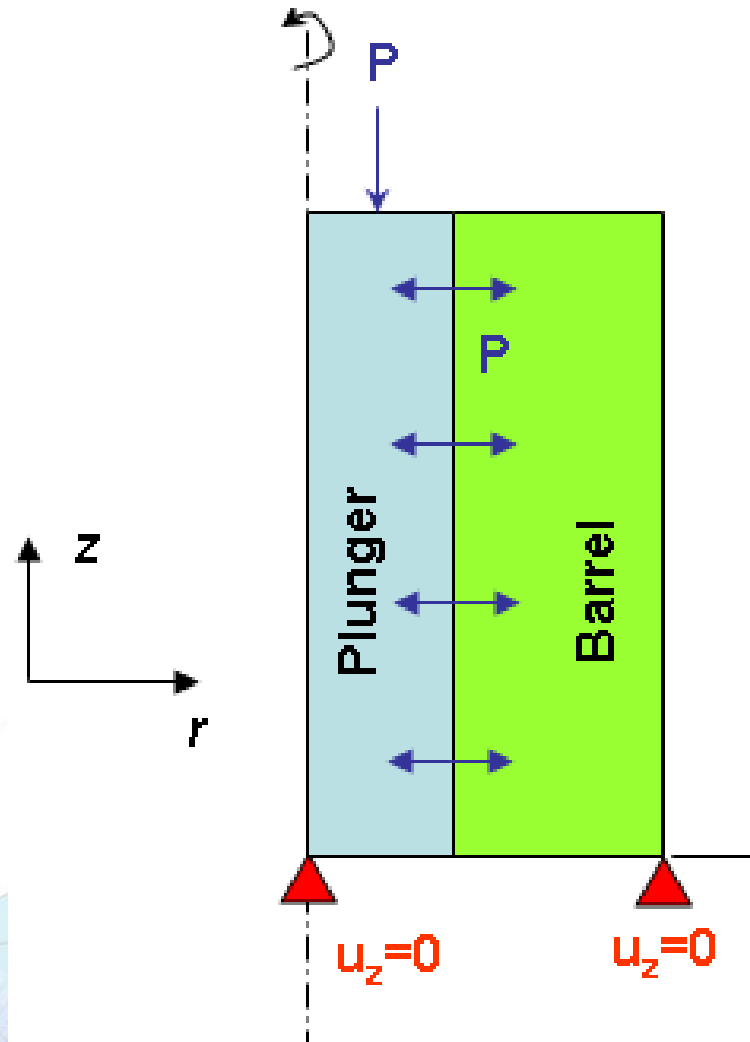
PTx is tangential derivative

Reynolds Equation - COMSOL

- Define expressions G_x , G_y , G_z for mass flow rate per unit width :

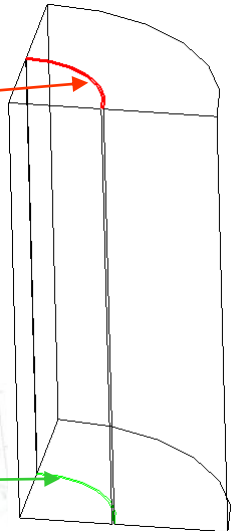
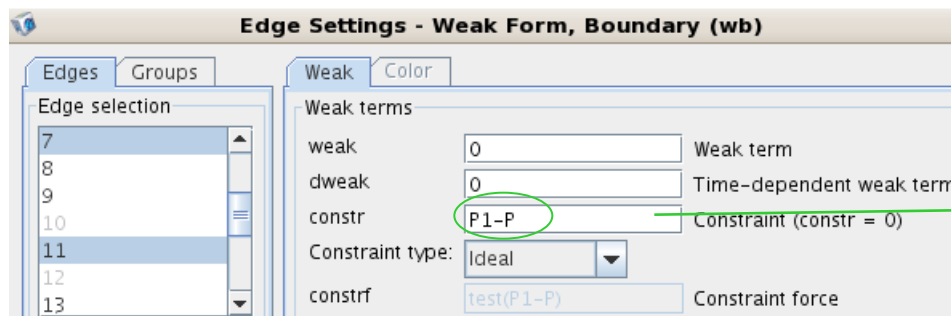
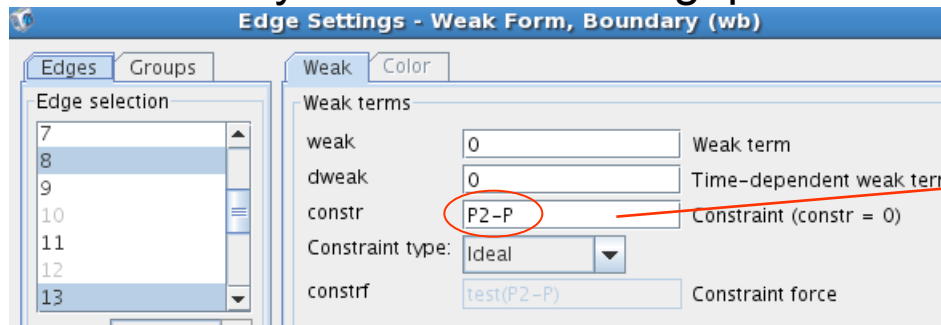
Global Expressions		
Name	Expression	Description
eta	visc(P,T)	viscosity P-T dependence
rho	rho_fluid(T,P/bar)	density P-T dependence
Gx	$\rho \cdot g^3 / (12 \cdot \eta) \cdot P T x - \rho \cdot g \cdot U0 / 2$	x-dir. mass flow rate per unit width, [kg/(m*s)]
Gy	$\rho \cdot g^3 / (12 \cdot \eta) \cdot P T y - \rho \cdot g \cdot V0 / 2$	y-dir. mass flow rate per unit width, [kg/(m*s)]
Gz	$\rho \cdot g^3 / (12 \cdot \eta) \cdot P T z - \rho \cdot g \cdot W0 / 2$	z-dir. mass flow rate per unit width, [kg/(m*s)]
mdot_x	$-Gx \cdot 2 \cdot \pi \cdot R$	mass flow rate in x-dir. [kg/s]
mdot_y	$-Gy \cdot 2 \cdot \pi \cdot R$	mass flow rate in y-dir. [kg/s]
mdot_z	$-Gz \cdot 2 \cdot \pi \cdot R$	mass flow rate in z-dir. [kg/s]

Axisymmetric Problem Setup



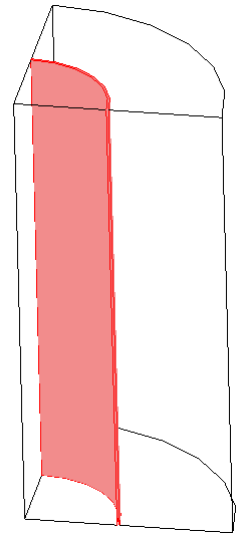
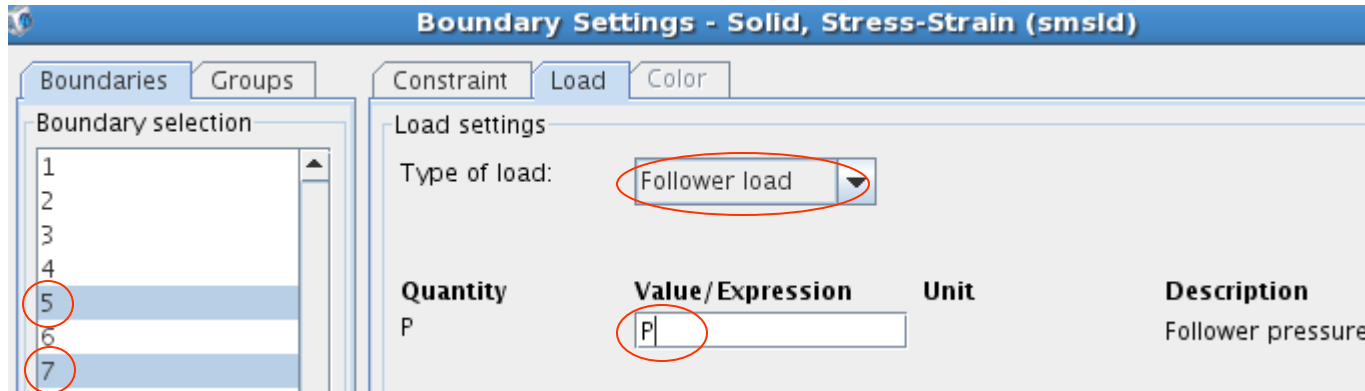
Reynolds Equation - COMSOL

- Define boundary conditions at the gap **entrance** and gap **exit** :

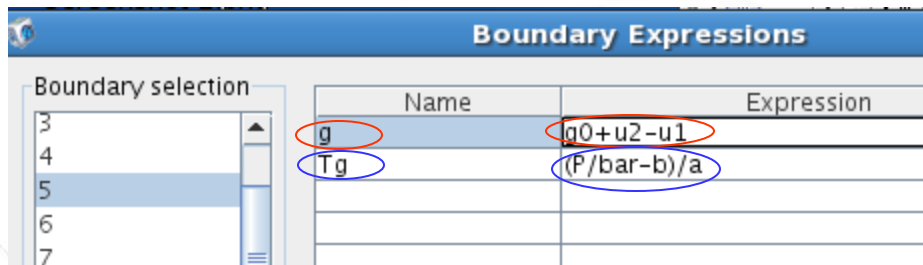


Reynolds Equation /Structural Analysis Coupling

- Apply Reynolds pressure to both surfaces of gap

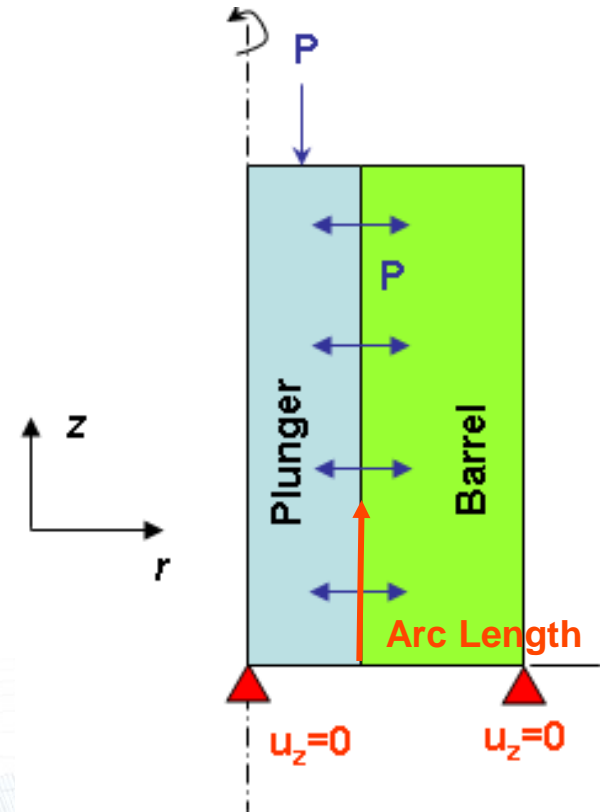
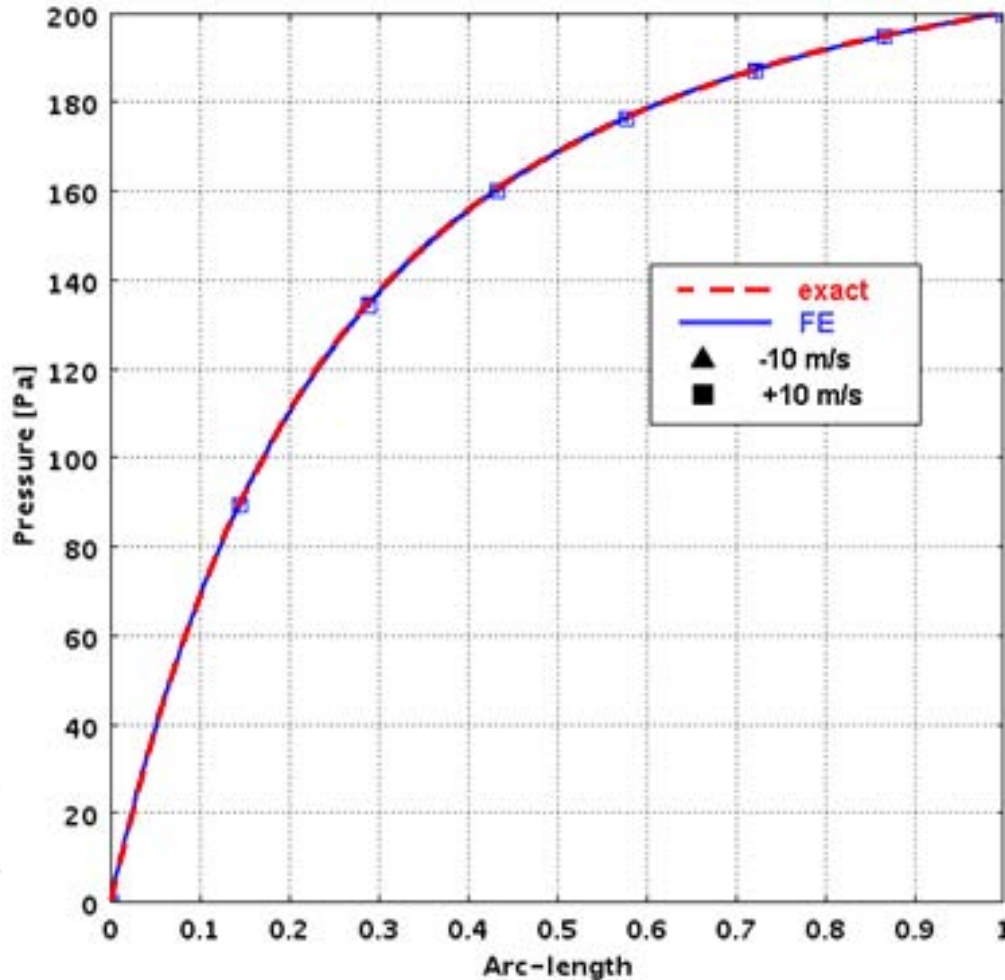


- Define **gap** using initial gap u_0 , displacement u_2 of gap OD, and displacement u_1 of gap ID

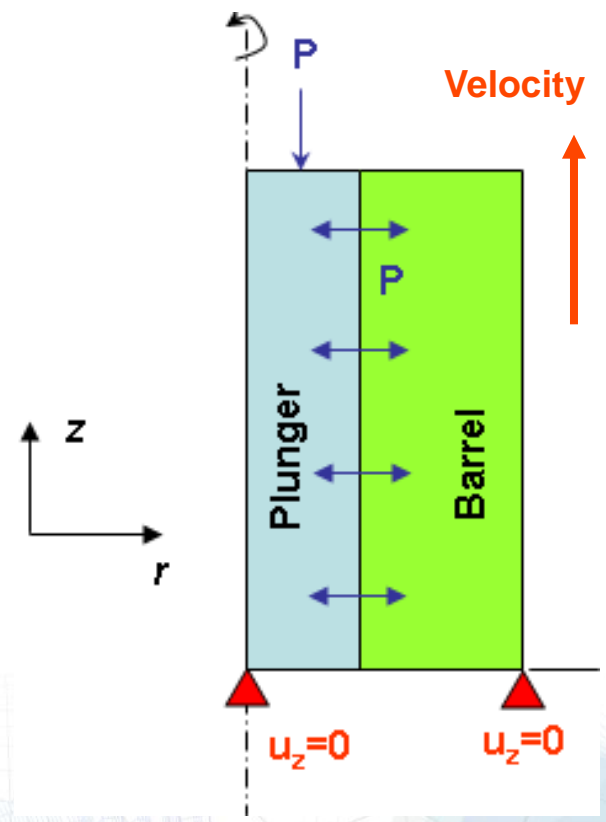
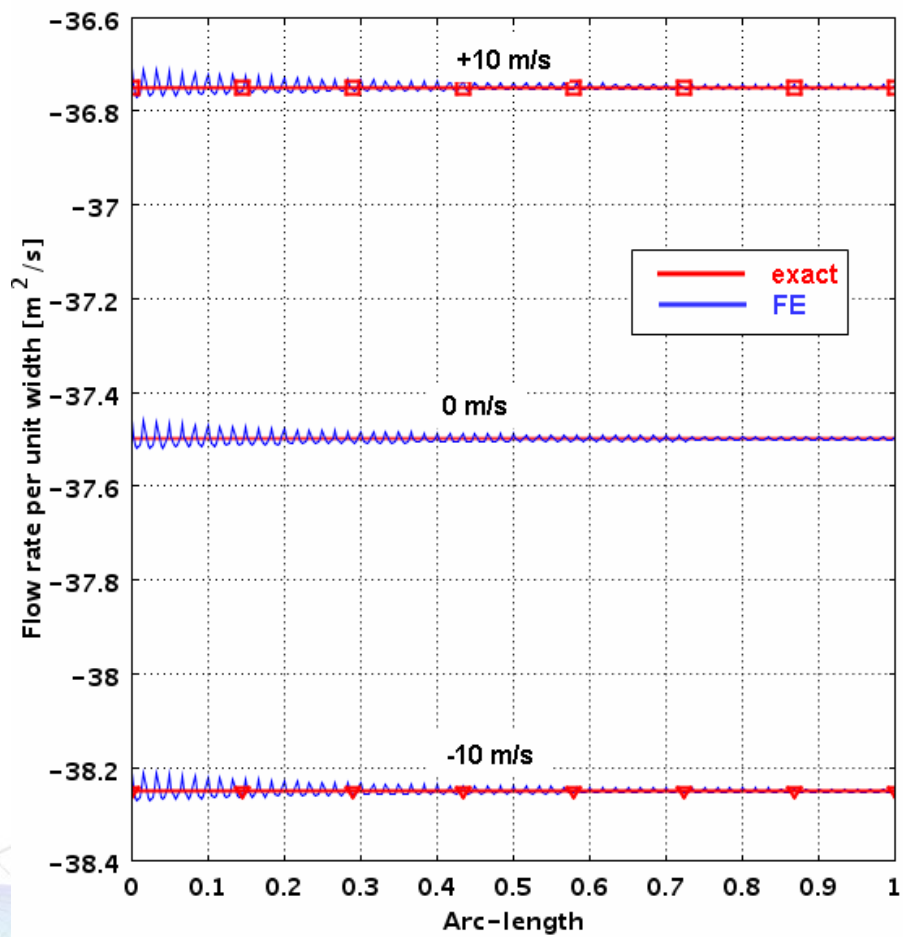


- Define temperature **Tg** along gap using relation $P=P(T, \text{enthalpy})$

Variation of Pressure along Path

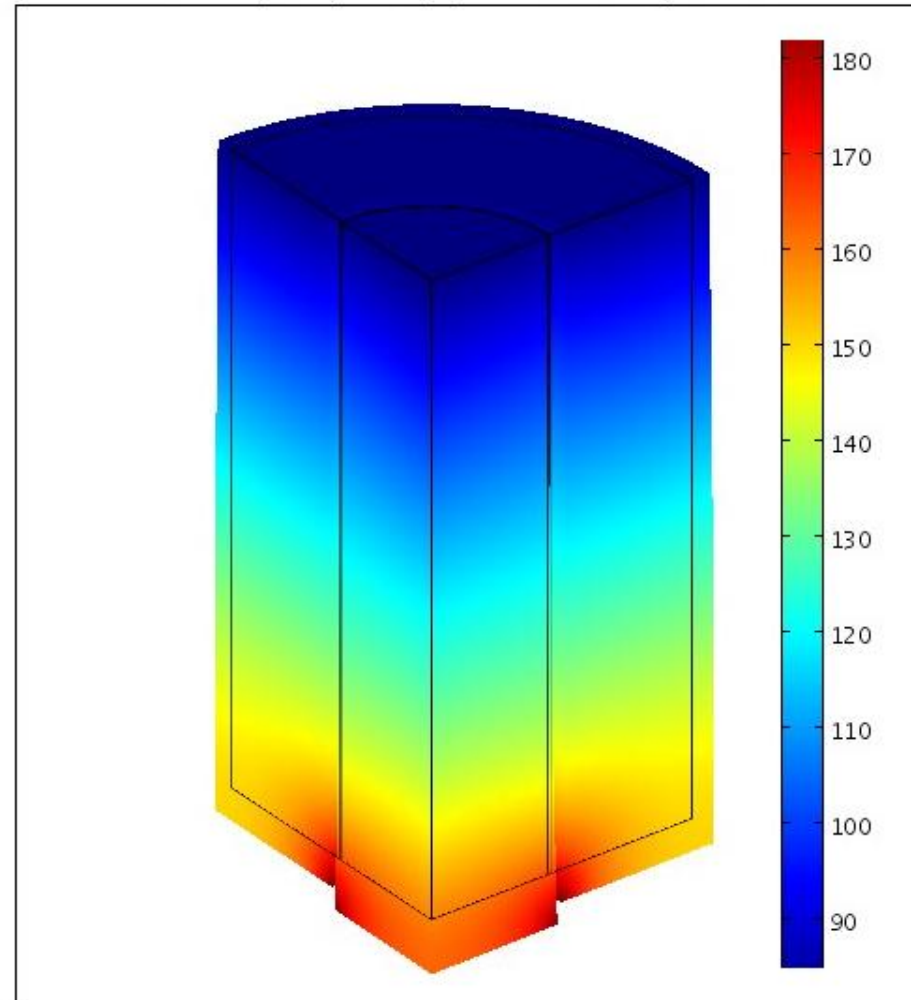


Effect of Velocity on Flow Rate



Temperature Distribution in Plunger/Barrel

Boundary: Temperature [K] Deformation: Displacement



Summary

- Analysis method developed that fully couples lubricant fluid flow with heat transfer and stress analysis
- Solution implemented in v3.5a
- Reynolds equations available in CFD Module in v4.0a
- Weak form methodology available in COMSOL Multiphysics without need for CFD module